Electrically tunable extraordinary optical transmission gratings

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We report a semiconductor based mechanism for electrically controlling the frequency of light transmitted through extraordinary optical transmission gratings. In doing so, we demonstrate active control over the surface plasmon (SP) resonance at the metal/dielectric interface. The gratings, designed to operate in the mid-infrared spectral range, are fabricated upon a doped GaAs epilayer. Tuning of over 25 cm\textsuperscript{-1} is achieved, and the devices are modeled to investigate the physical origin of the tuning mechanism. Though our structures are designed for the mid-infrared, the tuning mechanism demonstrated could be applied to other wavelength ranges, especially the visible and near infrared. © 2007 American Institute of Physics. [DOI: 10.1063/1.2804572]

Perforated metal films can exhibit extraordinary optical transmission (EOT) where, at certain wavelengths, more light passes through the sample than predicted by aperture theory.\textsuperscript{1} The majority of the work with EOT has been performed in the visible and near-infrared (near-IR) spectral regions. However, as mid-infrared (mid-IR, 3–30 \textmu m wavelength) sources steadily and rapidly improve, the burgeoning field of mid-IR photonics is presenting numerous opportunities for EOT technology and research. While current work with passive EOT structures has shown great promise, the ability to electrically tune such devices would add greater functionality to a variety of photonic applications. In previous work, we have shown that changing the carrier concentration in GaAs epilayers can shift the transmission peak of mid-IR EOT structures.\textsuperscript{2} For $n$-type doping densities varying from $1 \times 10^{16}$ to $3 \times 10^{18}$ cm\textsuperscript{-3}, a shift of 0.14 \textmu m (22 cm\textsuperscript{-1}) was achieved for gratings transmitting at 8 \textmu m (1250 cm\textsuperscript{-1}). While this previous work achieved EOT peak shifts utilizing separate samples, we show in this letter that even greater shifts can be achieved from a single device using electrically controlled current tuning of the EOT structure.

The sample studied, shown in Figs. 1(a) and 1(b), was grown by metal-organic chemical vapor deposition and consists of a 100 nm thick $n$-doped (3.5$ \times $10\textsuperscript{18} \text{cm}^{-3}$) GaAs epilayer above a undoped 50 nm Al\textsubscript{0.2}Ga\textsubscript{0.8}As epilayer and an undoped GaAs buffer layer on a semi-insulating GaAs substrate. Fabrication of the device, shown in Fig. 1(a), consisted of a mesa etch through the doped epilayer, followed by evaporation and annealing of Ohmic (235 A Ge/470 A Au/300 A Ni/1000 A Au) source and drain contacts. A 10 nm/50 nm Ti/Au square lattice grating designed for transmission at 8 \textmu m (2.4 \textmu m period and 1.25 \textmu m holes) was then defined using optical photolithography and a lift-off metallization process. While this is not an optimum metallization for mid-IR surface plasmons (SPs), previous work has shown that Ti/Au meshes exhibit EOT phenomena.\textsuperscript{2} Light transmission through such a structure relies on SP excitations at the air/metal and the metal/dielectric interfaces. An approximate expression for the normal incidence SP resonance condition, based on the SP dispersion of a smooth metal film, is given by\textsuperscript{3,4}

$$\sqrt{i^2 + j^2} \lambda = a_0 \Re \left( \frac{e_s e_m}{e_s + e_m} \right).$$ (1)

Here, $\lambda$ is the free space wavelength, $a_0$ is the lattice constant (2.4 \textmu m), $i$ and $j$ are integers related to the reciprocal lattice vectors $2\pi/a_0 x$ and $2\pi/a_0 y$, respectively, and $e_s$ and $e_m$ are the complex permittivities of the semiconductor (or air) and metal, respectively. The spectral position of the transmission peak related to the metal/semiconductor SP can be tuned by varying $a_0$ or $e_s$. When current is passed under the metal mesh, as shown in Fig. 1(c), the epilayer is resistively heated, tuning both of these parameters, to varying degrees, simultaneously.

The normalized mid-IR transmission for our device as a function of electrical current is displayed in Fig. 2. Mid-IR transmission data was collected with a Fourier transform infrared spectrometer using an external, liquid-nitrogen cooled mercury cadmium telluride detector. Spectral resolution of 2 cm\textsuperscript{-1} was used and the data was averaged over 25 scans.

FIG. 1. (Color) Tunable midinfrared extraordinary transmission device. (a) Optical micrograph of tunable EOT device with labeled source contact (S), drain contact (D), and grating. (b) Scanning electron micrograph of transmission grating designed for transmission at 8 \textmu m. (c) Schematic of tunable EOT device showing current path through $n$-doped GaAs epilayer, source and drain contacts, and transmission grating (not to scale).

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Current was applied between the source and drain contacts using a dc power supply operating in constant current mode. Data collection was initiated upon stabilization of the source-drain voltage (approximately 1 – 5 s). The transmission spectra exhibit the Fano-lineshape associated with EOT structures. The relatively large background signal (~84%) is due to the light transmission through the nonmetallized areas that can be seen in Fig. 1(a) along the perimeter of the Ohmic contacts and the mesh. A transmission peak redshift of approximately 25 cm⁻¹ is achieved as the source-drain current is tuned from 0 to 200 mA (0 to 1.86 W power dissipated). The strength of the transmission peak does not decrease substantially (~25% reduction) at the highest current. Additionally, we see no increase in the peak linewidth as a function of current. Both of these results suggest that scattering and free carrier losses do not significantly affect device performance at high temperatures. The tuning achievable with such a configuration, in addition to the stable transmission strength and linewidth, suggests that such devices could be utilized as actively tunable mid-IR optical components.

A number of mechanisms are associated with temperature changes that can cause the observed shift. To accurately model these, the temperature of the device as a function of current must be determined. Temperature calibration was obtained by band edge photoluminescence (PL) spectroscopy. As the current is increased and the sample is heated, the semiconductor band edge shifts, as shown in the inset of Fig. 3. By tracing the position of the GaAs band edge PL as a function of current, an approximate value for the device temperature is found using the empirical relation for the temperature (Kelvin) dependence of the GaAs band gap (eV),

\[ E_g(T) = 1.519 - 5.405 \times 10^{-2}T^2/(T + 204). \]  

As shown in Fig. 3, the temperature of the device can be tuned from 300 K (0 mA) to over 550 K (200 mA).

From a geometrical standpoint, thermal expansion can change \( \omega_0 \) which, according to Eq. (1), would lead to a redshift in the SP transmission peak. However, this is only a small effect (~2 cm⁻¹) at the highest temperatures. In our semiconductor medium, there are several competing temperature dependent dielectric shifts. In the undoped material, we must consider the thermal generation of free carriers and the temperature dependence of the dielectric constant. In the relatively thin doped layer, which contains a high density of built-in free carriers, these effects must be considered along with the reduction of both the semiconductor plasmon damping term and the free carrier effective mass. The thin Al₀.₇Ga₀.₃As layer, having optical properties very similar to GaAs (Ref. 7) (and because it is very thin compared to the wavelengths of interest), is modeled together with the undoped GaAs buffer layer for simplification.

The temperature dependence of the semiconductor dielectric function can be modeled using the Drude approximation, including scattering, as

\[ \varepsilon(\omega, T, n) = \varepsilon_b(T) \left[ 1 - \frac{\omega_p(T,n)^2}{\omega^2 + i \omega \gamma(T, n)} \right], \]

\[ \omega_p(T,n)^2 = \frac{4 \pi n(T) e^2}{\varepsilon_b(T)m^* (T, n)}. \]  

Here, \( \omega_p(T,n) \) is the plasma frequency, \( \gamma(T, n) \) is the plasmon damping term (~1/\( \tau \), where \( \tau \) is the scattering time), \( n(T) \) is the carrier concentration, \( e \) is the charge of an electron, \( \varepsilon_b(T) \) is the background high frequency dielectric constant of the semiconductor, and \( m^* (T, n) \) is the effective electron mass in the semiconductor. In Fig. 4(a), the shift of the SP resonance is modeled using Eq. (1) with a Au mesh and the temperature and doping dependent relationships for the above parameters \( m^* , \omega_p, \gamma, n, \) and \( \varepsilon_b \).

The modeled shift is greatest for the undoped GaAs buffer and substrate, and is explained by the temperature dependence of the GaAs dielectric constant,

\[ \varepsilon_b(T) = 10.6(1 + T \cdot 9 \times 10^{-5}). \]  

Thermal generation of carriers can only create bulk densities on the order of \( 1 \times 10^{13} \text{ cm}^{-3} \) at our elevated temperatures, which is orders of magnitude too low to provide any noticeable shifting of the SP peak. The additional temperature dependent terms in Eq. (3) do, however, affect the peak position expected at higher temperatures for doped material. In Fig. 4(a), as the doping of the semiconductor is increased, the redshift of the transmission peak is somewhat offset by the Drude contribution to the dielectric function.

Figure 4(b) shows the calculated redshift for an 8 µm grating device (black dashed) assuming an undoped GaAs dielectric along with the measured peak positions (red). Since the redshift in our devices is greater than that predicted by temperature tuning of the undoped dielectric, it is argued that the majority of the metal/semiconductor SP field lies in the semiconductor.

FIG. 2. (Color) Transmission spectra showing peak shift with current. Normalized transmission spectra for 8 µm tunable surface plasmon device as a function of source-drain current. A clear redshift can be seen as the current is increased from 0 to 200 mA. The maximum shift achieved was 25 cm⁻¹.

FIG. 3. (Color) Device surface temperature derived from photoluminescence spectra (inset) as a function of current. For a fixed current, photoluminescence was used to relate the position of the GaAs band edge to the device temperature. The main plot shows the resulting temperature calibration obtained using this method.
the undoped material, and the thin, highly doped GaAs layer serves mostly as a heating mechanism with minimal influence over the SP transmission peak spectral position.

To utilize these tunable plasmonic devices as active optical components, the effect of losses on the transmission intensity and the linewidth of the transmission peak must be addressed. As mentioned earlier, a decrease in transmission peak strength of ~25% is seen as the device temperature is increased. This is most likely due to increased losses in both the 500 µm GaAs substrate and at the interface between the metal mesh and the highly doped GaAs epilayer. Burying the doped GaAs layer under an undoped surface layer would decrease the overlap of the SP field with the free carriers of the doped layer, while still allowing for resistive heating of the sample. Substrate losses can be minimized by moving toward thinner devices which, at the same time, will reduce the thermal mass and electrical power requirements. Finally, the linewidth and shape of the transmission peak can also be significantly improved by utilizing the crossed-polarizer experimental configuration employed by Pang et al.\textsuperscript{5} We have performed such an experiment on large area SP gratings and have seen linewidths of less than 10 cm\textsuperscript{-1} for EOT gratings designed for transmission at 9 µm (1111 cm\textsuperscript{-1}).

In conclusion, we have demonstrated electrically controlled temperature tuning of transmission through extraordinary optical transmission gratings in the midinfrared. We have shown tuning of over 25 cm\textsuperscript{-1} by adjusting the current beneath the metal/dielectric interface. The dielectric properties of both the doped heater layer and the undoped substrate were analyzed in order to understand the origins of the transmission tuning. The development of semiconductor based tuning mechanisms for mid-IR SP resonances is important for a variety of active mid-IR photonic devices including filters, emitters, and detectors. However, it should be noted that this work has implications for a broad range of frequencies, as the mechanisms investigated could be utilized in the near-IR and visible (with a wide band gap semiconductor) wavelength ranges. The ability to design and fabricate active, electrically controlled, surface plasmon devices in the mid-IR and possibly the near-IR/visible range opens up new capabilities for plasmon-based technologies.

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