



CIVE.5120 Structural Stability (3-0-3)
04/04/17



Buckling of Beams – II

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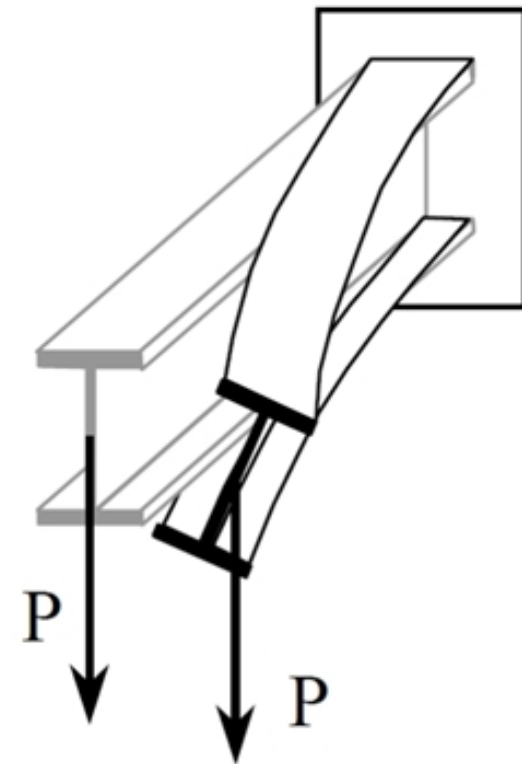
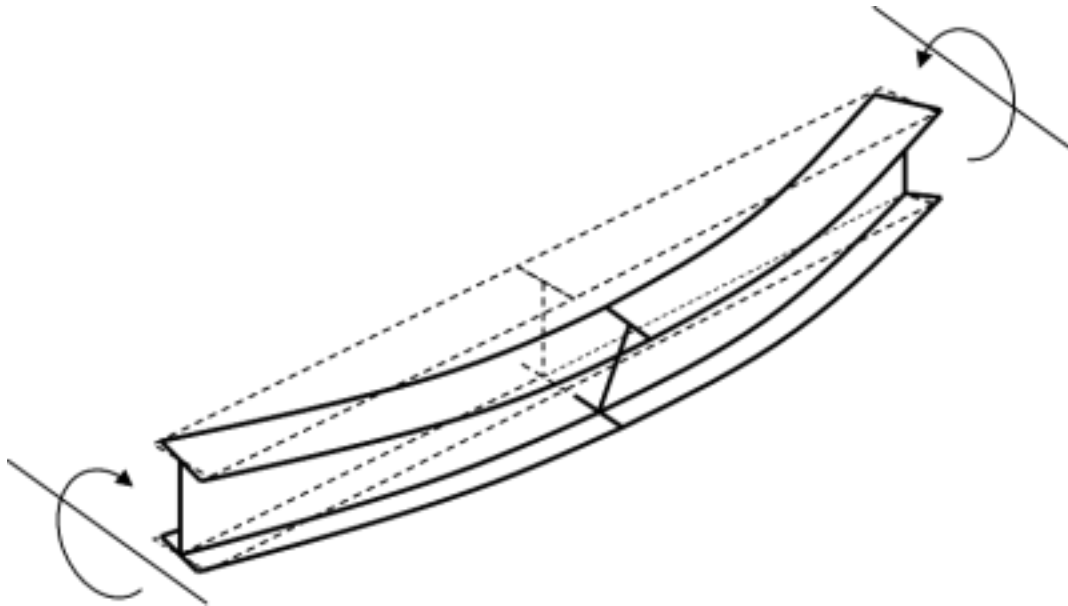
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Outline

- Analysis of lateral buckling of beams
 - Simply-supported I-beam under a central concentrated load
 - Simply-supported I-beam under a uniformly distributed load
 - Out-of-plane bending and torsional buckling of doubly symmetric sections
 - Continuous beams
- Effect of the location of loading
- Review on the determination of the shear center
- Effect of boundary condition
- Summary

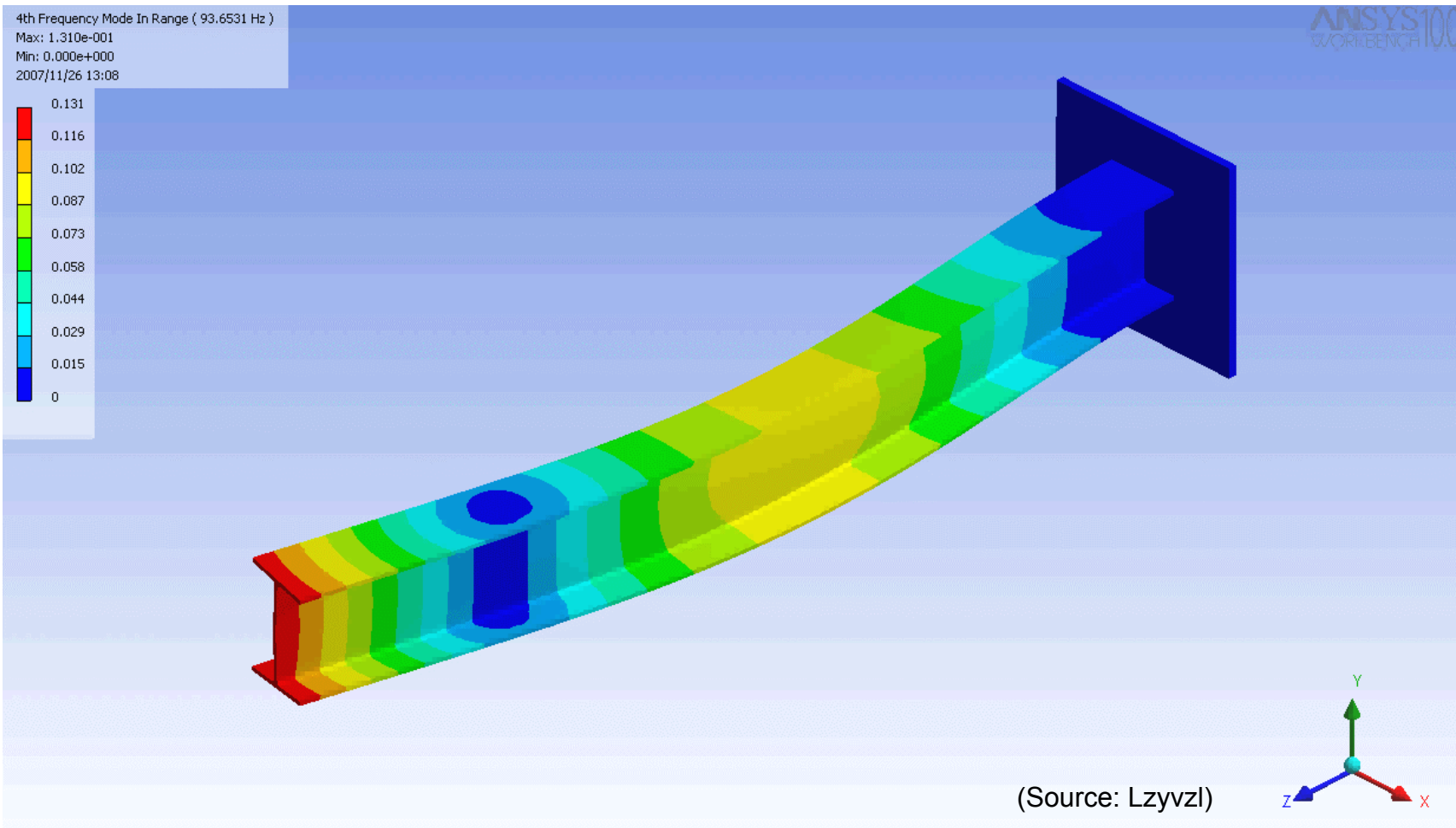
Beams – II

- Analysis of lateral buckling of beams



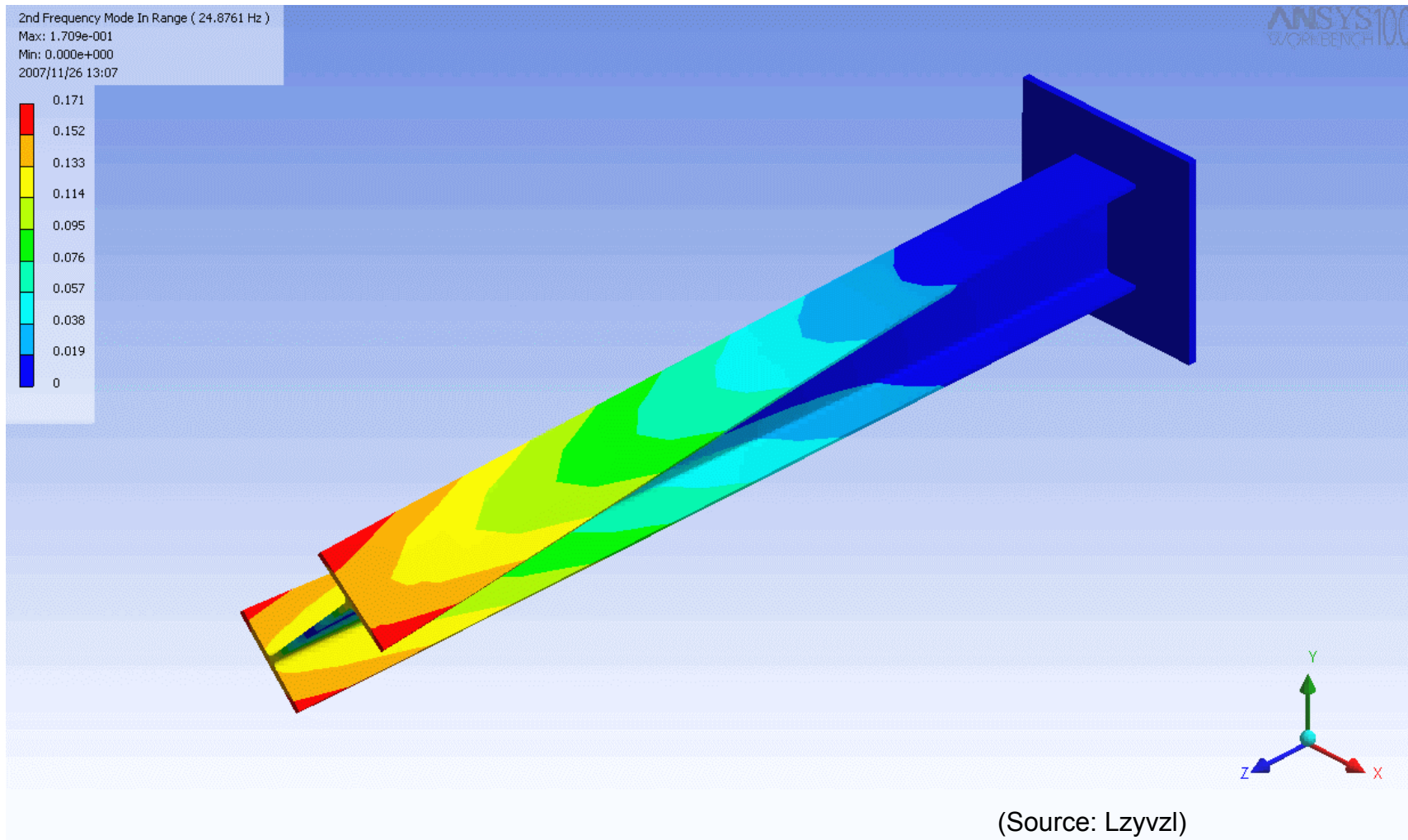
Beams – II

- Analysis of lateral buckling of beams – Stress-distribution



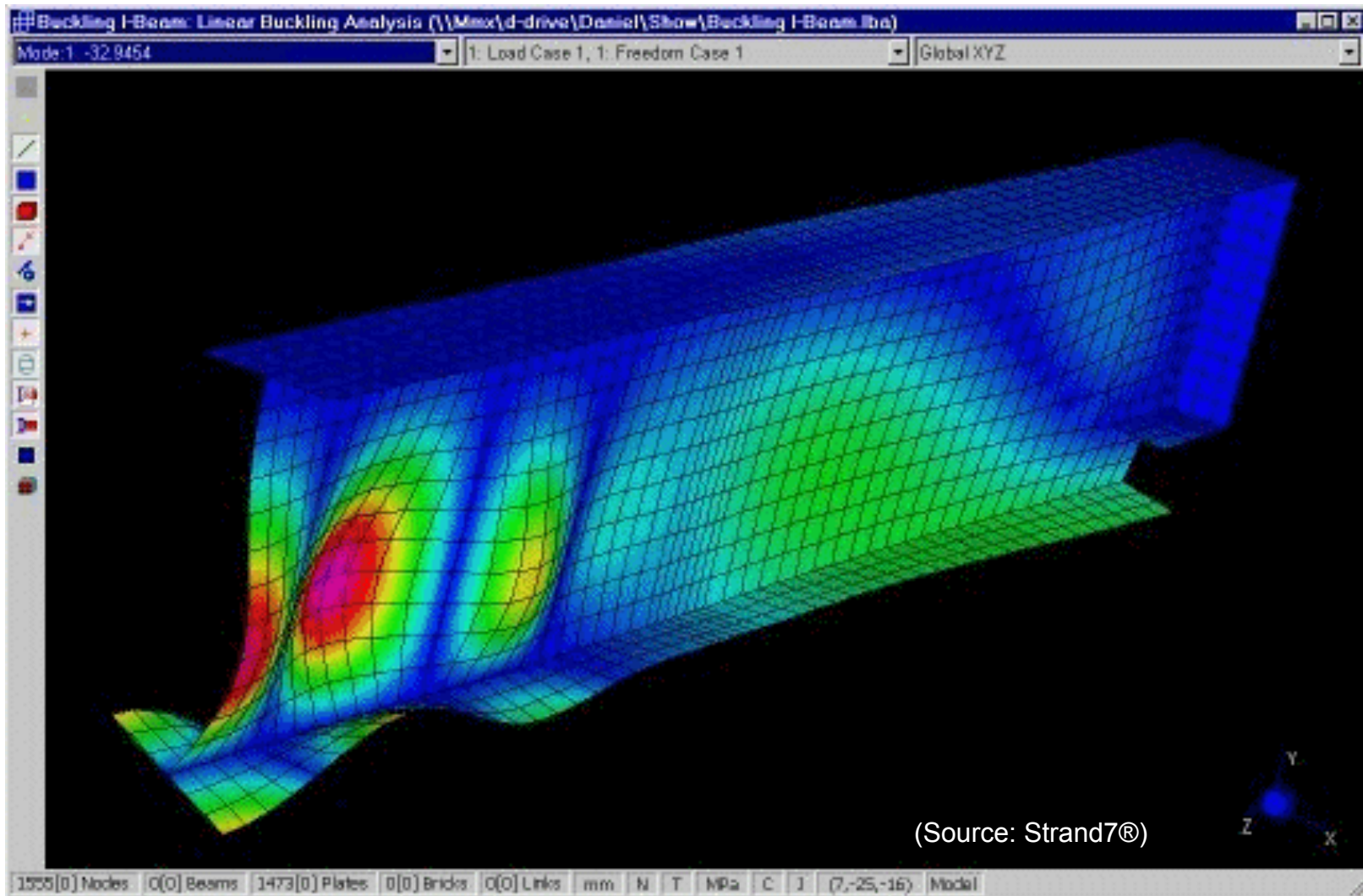
Beams – II

- Analysis of lateral buckling of beams – Stress-distribution



Beams – II

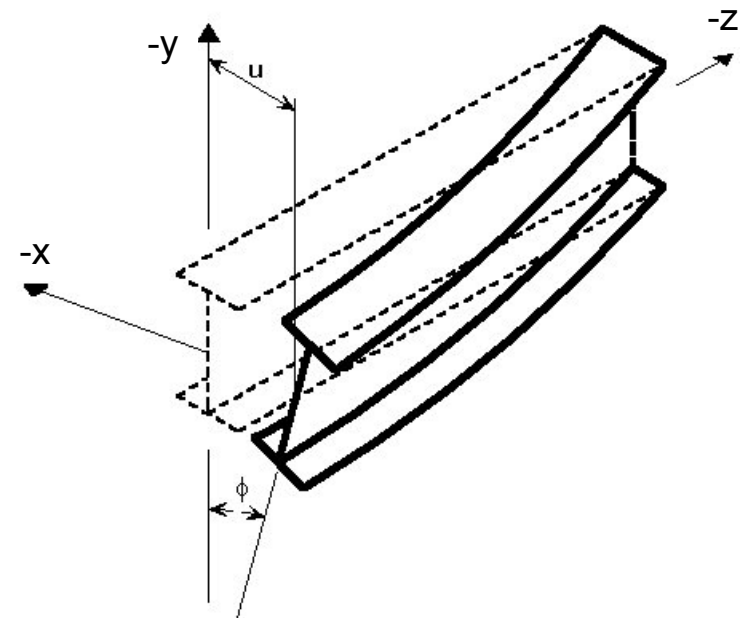
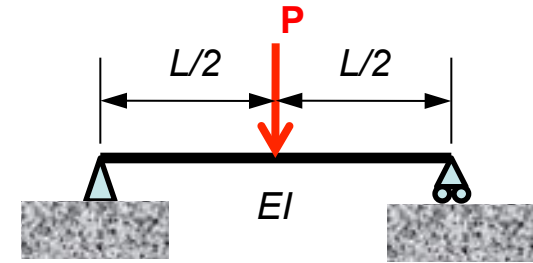
- Analysis of lateral buckling of beams – Stress-distribution



Beams – II

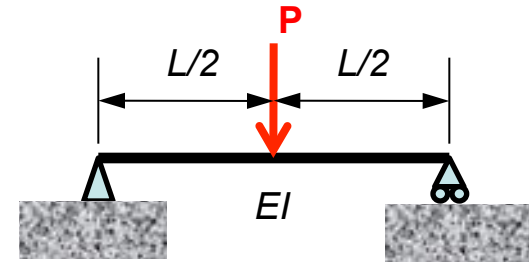
- **Analysis of lateral buckling of beams**

- Simply-supported **I-beam** under a central concentrated load
 - Governing equations
 - In-plane bending
 - Out-of-plane bending
 - Torsion
 - Characteristic equation of the system



Beams – II

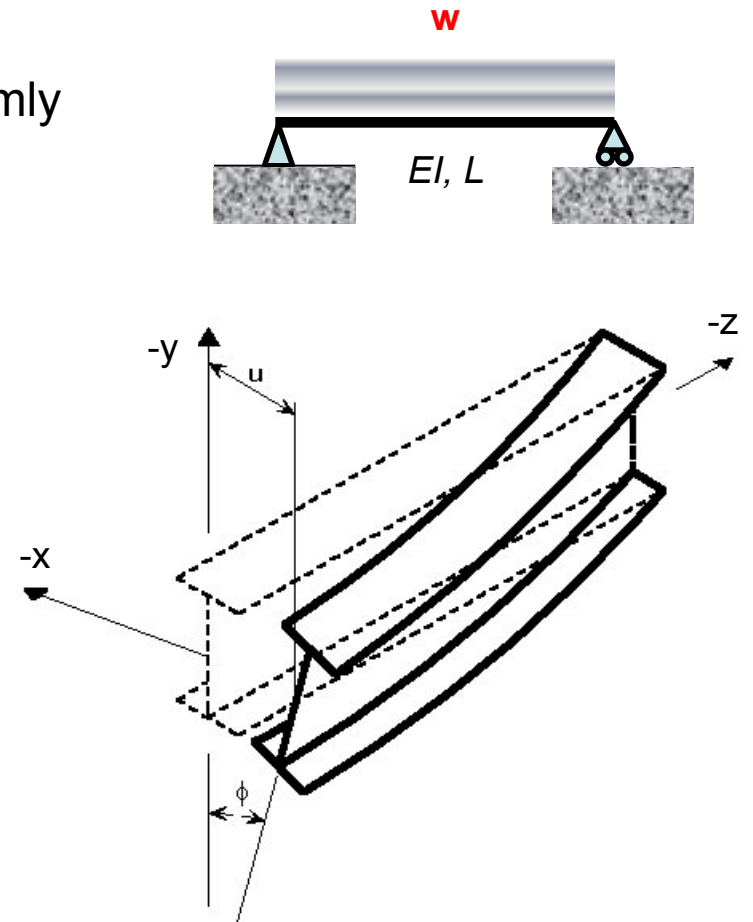
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 - B.C.
 - Solution of the critical moment



Beams – II

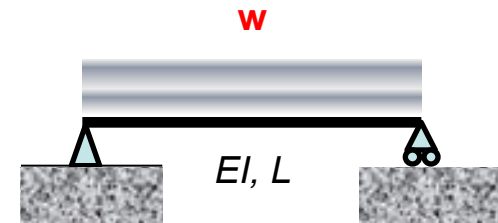
- **Analysis of lateral buckling of beams**

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Beams – II

- **Analysis of lateral buckling of beams**
 - Simply-supported **I-beam** under a uniformly distributed load
 - B.C.
 - Solution of the critical moment



Beams – II

- **Analysis of lateral buckling of beams**
 - Out-of-plane bending and torsional buckling of doubly symmetric sections (Clark and Hill 1962)

Beams – II

- **Analysis of lateral buckling of beams**
 - Continuous beams

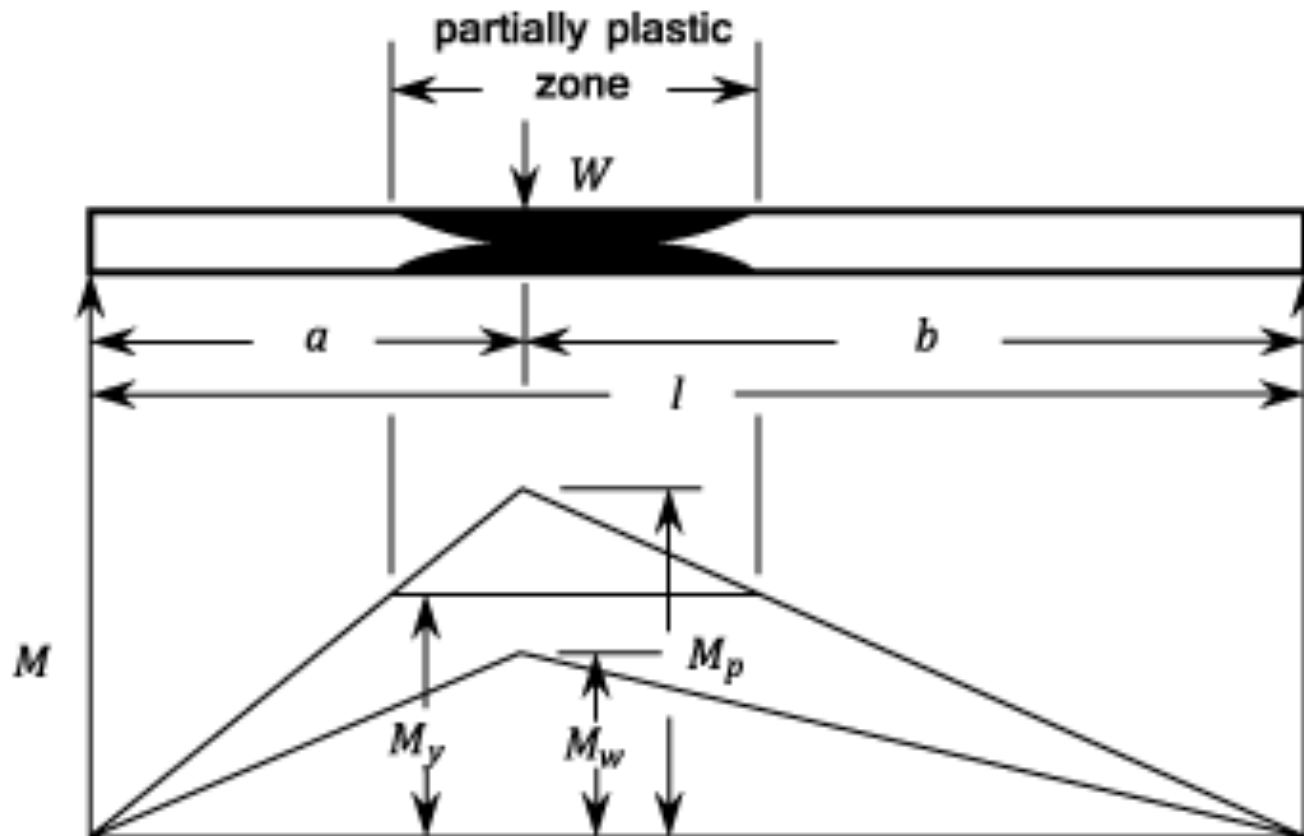
Beams – II

- **Effect of the location of loading**
 - Above the shear center
 - At the shear center
 - Under the shear center

Q: How does this phenomenon affect the design of beams for lateral torsional buckling?

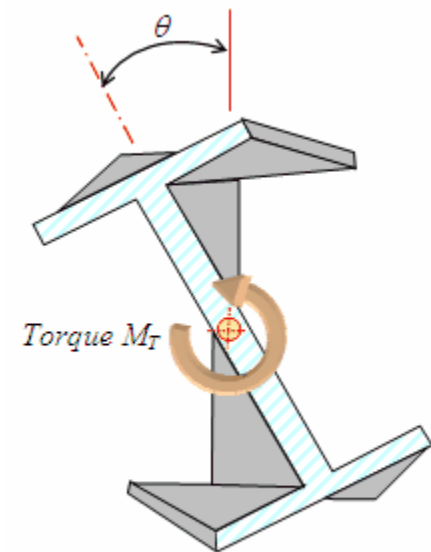
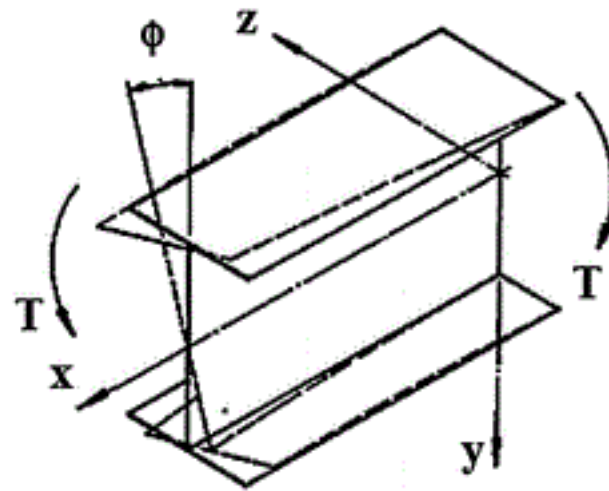
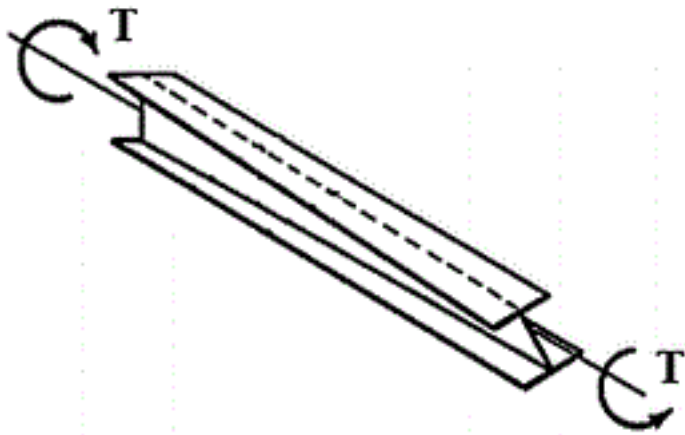
Beams – II

- Formation of plastic hinge on a steel I-beam cross section



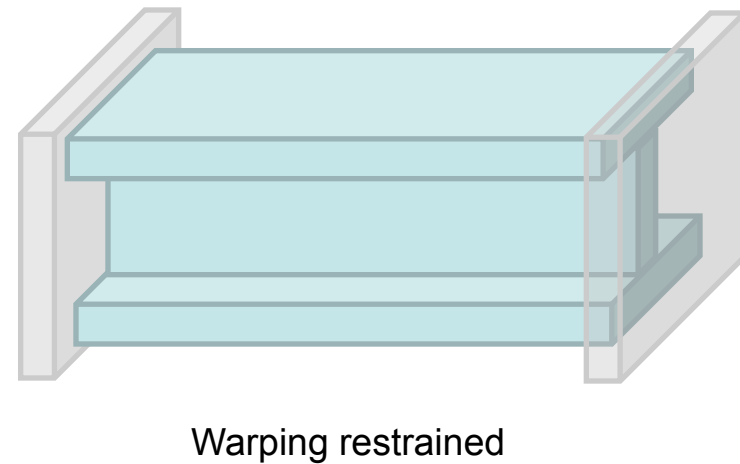
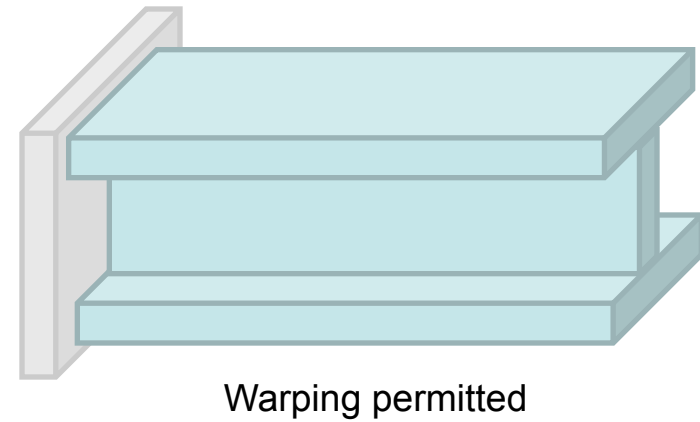
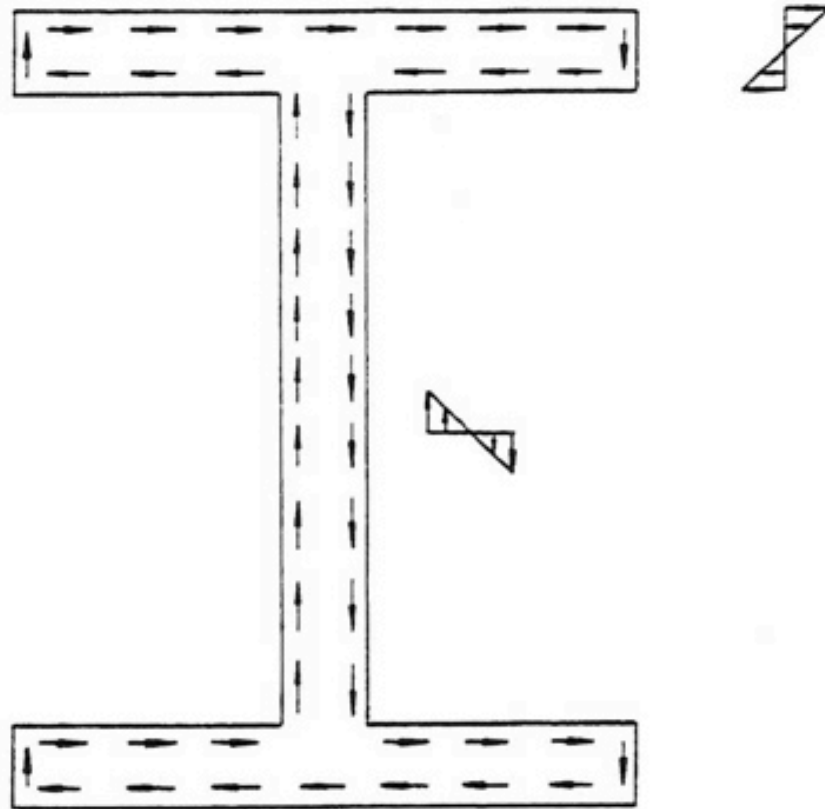
Beams – II

- Uniform torsion of thin-walled open sections



Beams – II

- Venant shear stress distribution in an I-section

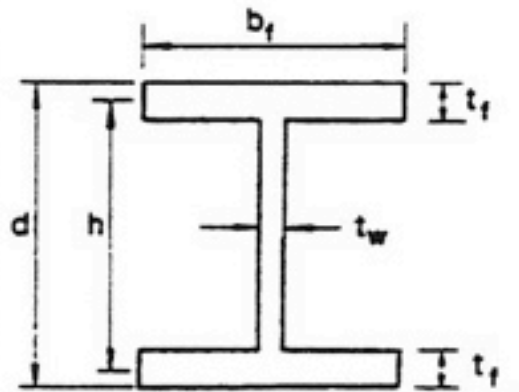


*If warping restrained at the support,
Venant shear will be developed.*

Beams – II

- Warping constant, C_w

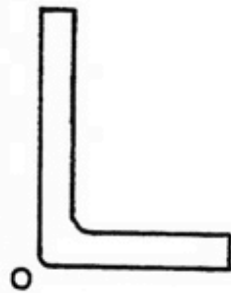
Table 5.1 Torsional Constant and Warping Constant for a Doubly Symmetric I-Section

 <p>The diagram shows a cross-section of a doubly symmetric I-beam. The total depth is labeled 'd', the web height is 'h', the flange width is 'b_f', the flange thickness is 't_f', and the web thickness is 't_w'. The beam is symmetric about both the vertical and horizontal axes.</p>	<p>Torsional Constant</p> $J = \frac{2b_f t_f^3 + (d - 2t_f) t_w^3}{3}$	<p>Warping Constant</p> $C_w = \frac{t_f b_f^3 h^2}{24}$
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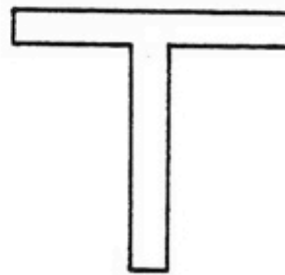
Beams – II

- Cross sections without any Venant shear stress ($C_w = 0$)

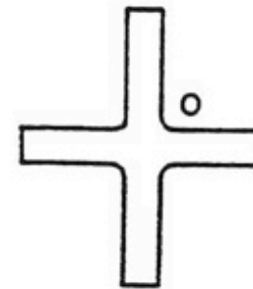
FIGURE 5.9 Cross sections with $C_w = 0$



Angle

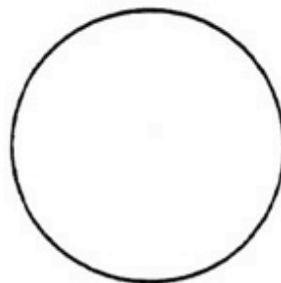


Tee

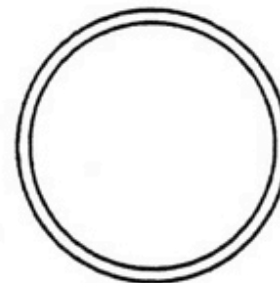


Cruciform

(a)



Solid Circular



Tubular

(b)

Beams – II

- Equivalent moment factor, C_b

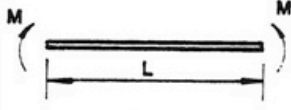
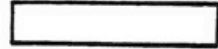
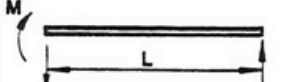

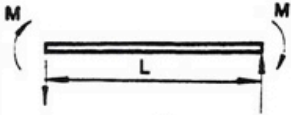

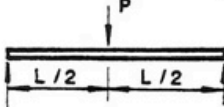

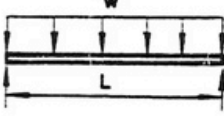

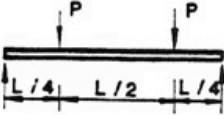
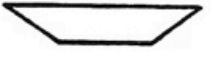
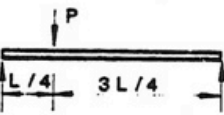

Loadings	Bending Moment Diagrams	M_{cr}	C_b
		M_{cr}	1.00
		M_{cr}	1.75
		M_{cr}	2.30
		$\frac{P_{cr} L}{4}$	1.35
		$\frac{w_{cr} L^2}{8}$	1.13
		$\frac{P_{cr} L}{4}$	1.04
		$\frac{3 P_{cr} L}{16}$	1.44

Table 5.2 Values of C_b for different loading cases (all loads are applied at shear center of the cross section)

Beams – II

- Effect of the location of a concentrated load on an I-beam

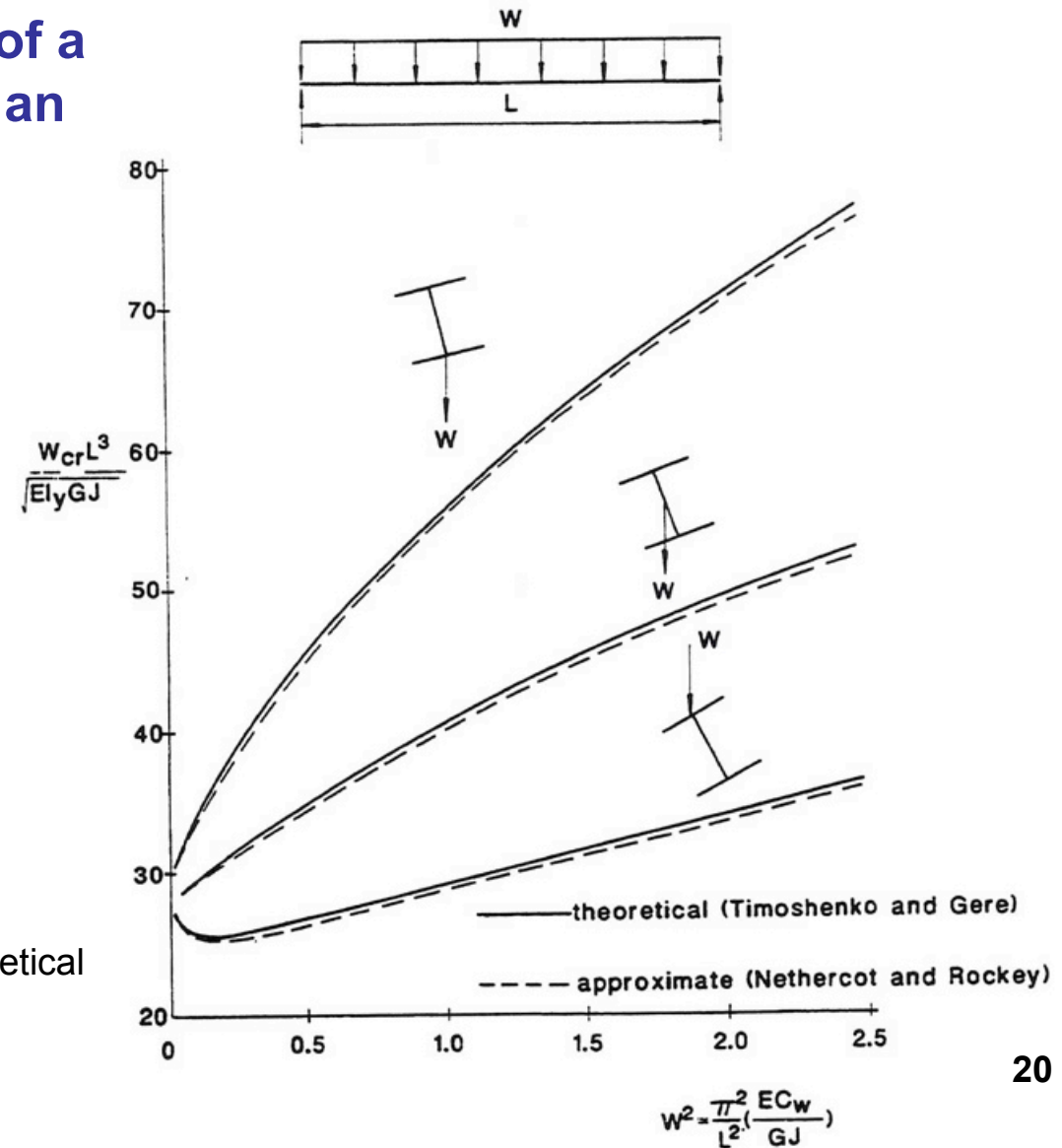
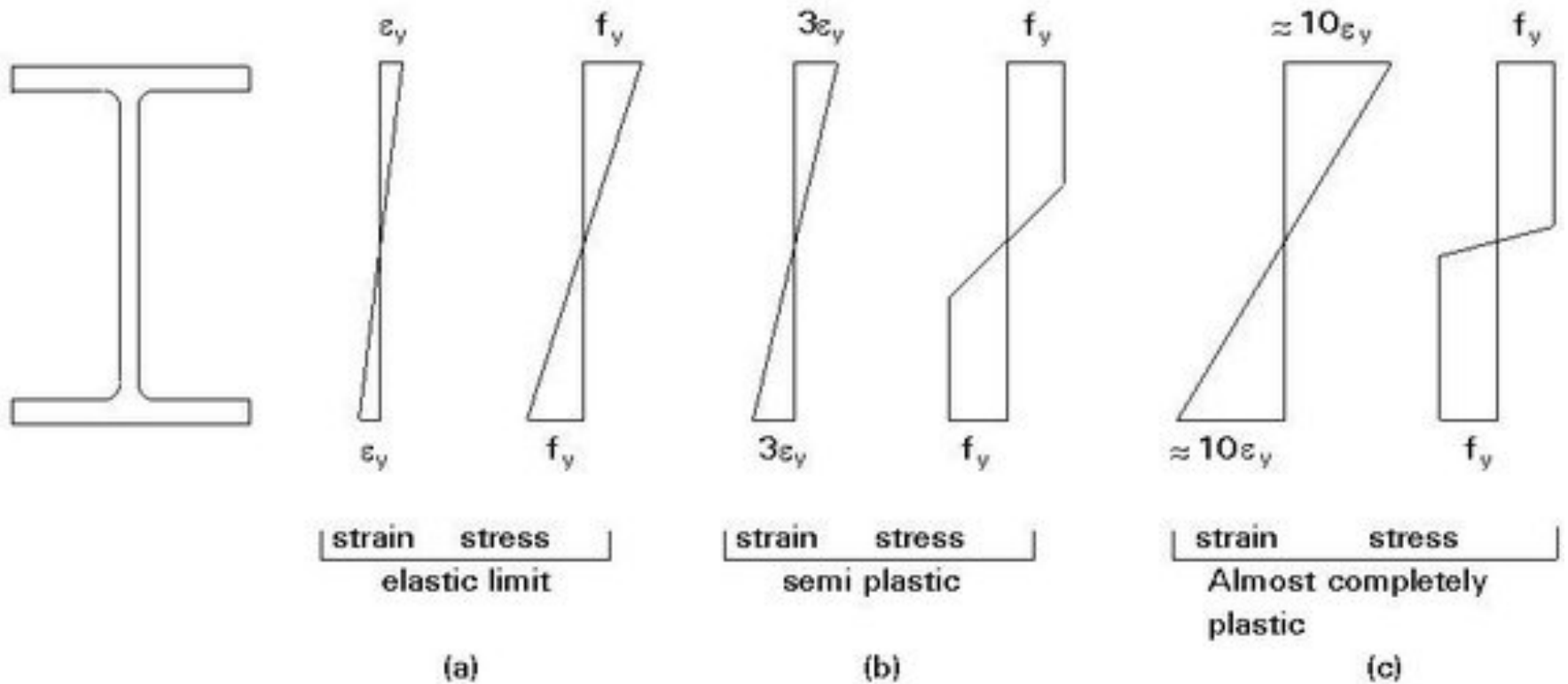


FIGURE 5.19 Comparison of theoretical and approximate solutions

Beams – II

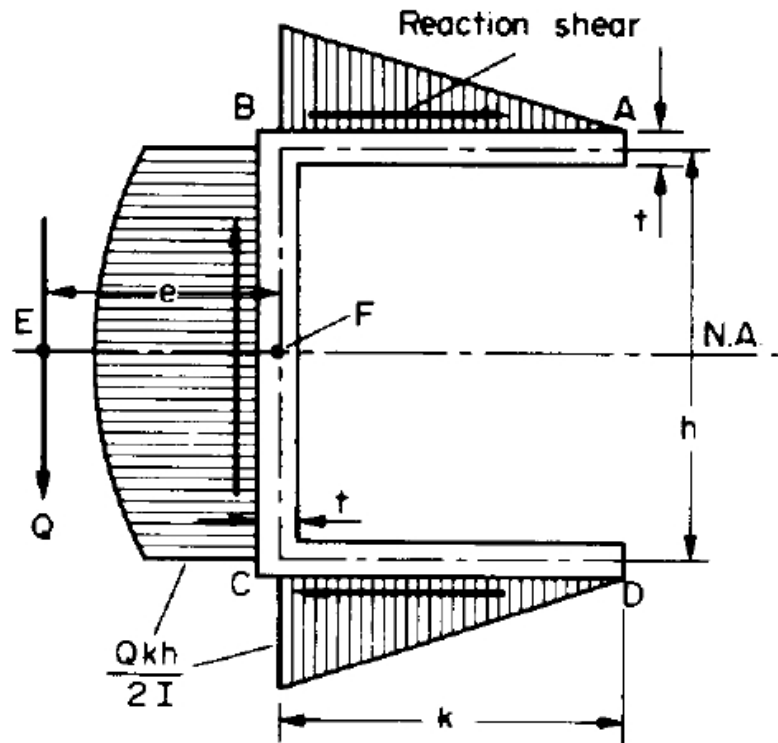
- Formation of plastic hinge on a steel I-beam cross section



Beams – II

- **Review – Determination of the shear center**

- Definition: The shear center of a section is the location at which the application of a concentrated load will result in zero twist of the section.
- Example: Channel section beams



$$\tau_B = \frac{QA\bar{y}}{It} = \frac{Q \times kt}{It} \times \frac{h}{2} = \frac{Qkh}{2I}$$

$$\tau_A = 0$$

$$\text{Average stress} \times \text{area} = \frac{1}{2} \times \frac{Qkh}{2I} \times kt = \frac{Qk^2ht}{4I}$$

$$Q \times e = \frac{Qk^2ht}{4I} \times h$$

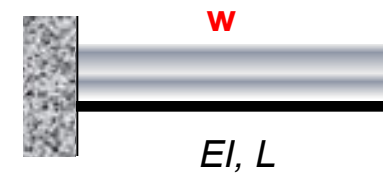
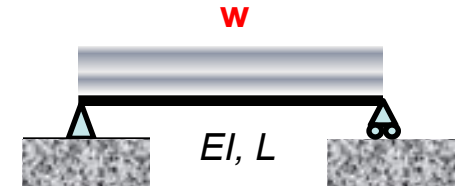
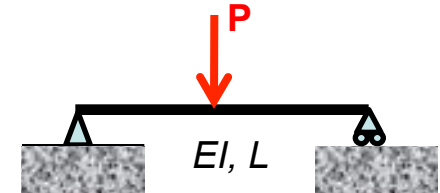
$$e = \frac{k^2h^2t}{4I} \rightarrow \text{Shear center}$$

(Source: E.J. Hearn (1997))

Beams – II

- **Effect of boundary conditions**

- Simply-supported, concentrated load
- Simply-supported, uniformly distributed load
- Cantilever (one end fixed and the other free), uniformly distributed load
- Fixed-ended, equal end moments



Beams – II

- **Effect of boundary condition**

- Asymmetric boundary conditions
 - Warping prevented in one plane and bending permitted in another plane



Bending permitted



Twisting permitted but warping prevented

- Concept of the effective length KL

Summary

- The boundary condition of beams can be considered by different values of the effective length, KL , which depends on
 - Unbraced length of the beam
 - Material properties E and G ,
 - Cross-section geometry c_w and J ,
 - Types of loadings
 - Location of the load w.r.t. the shear center of the cross section.
- For design purpose, it is conservative to evaluate the critical load for each span in a continuous beam by assuming the ends of the span are simply supported.