

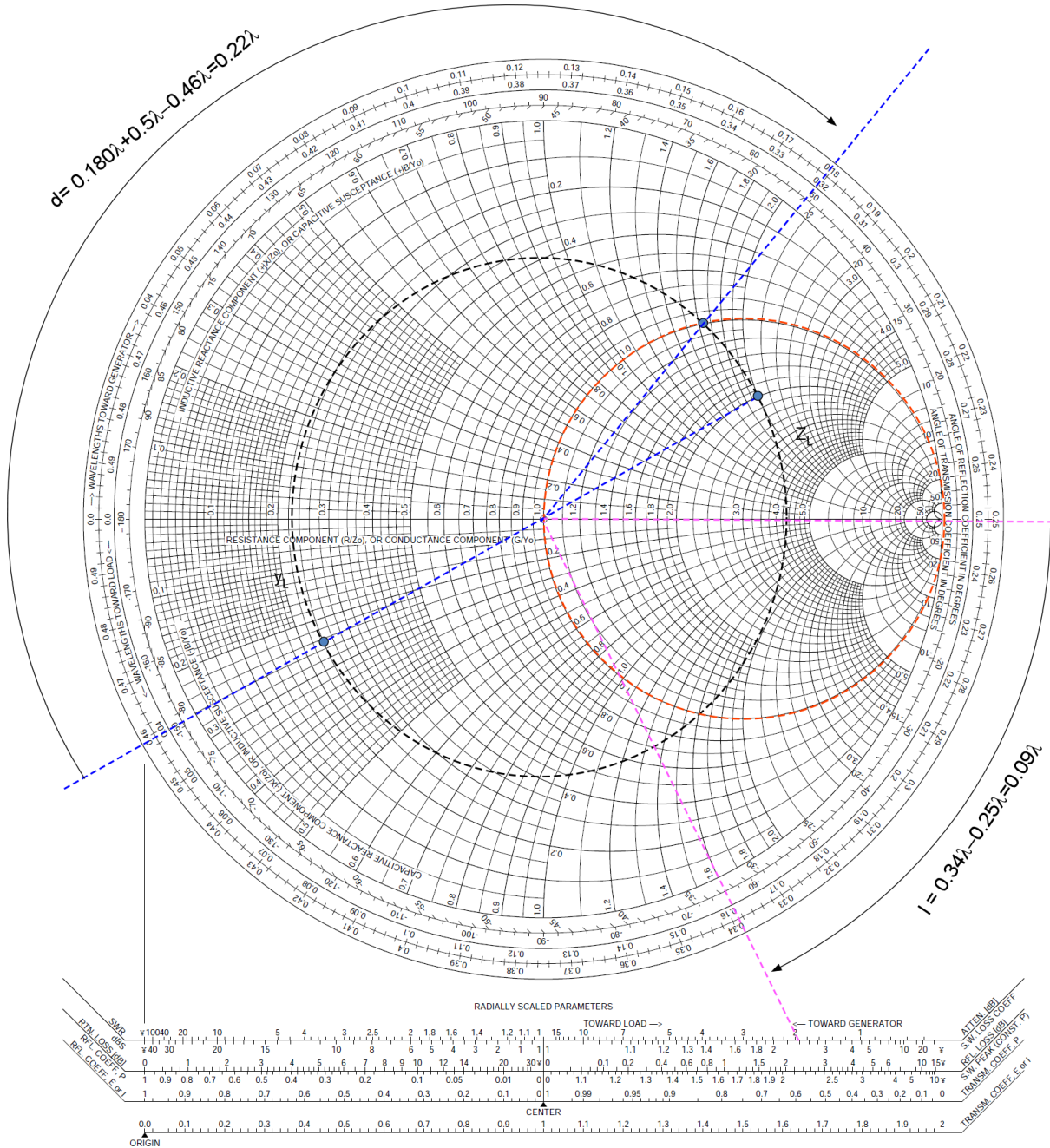
EECE.3600 Final Exam

12/16/2016

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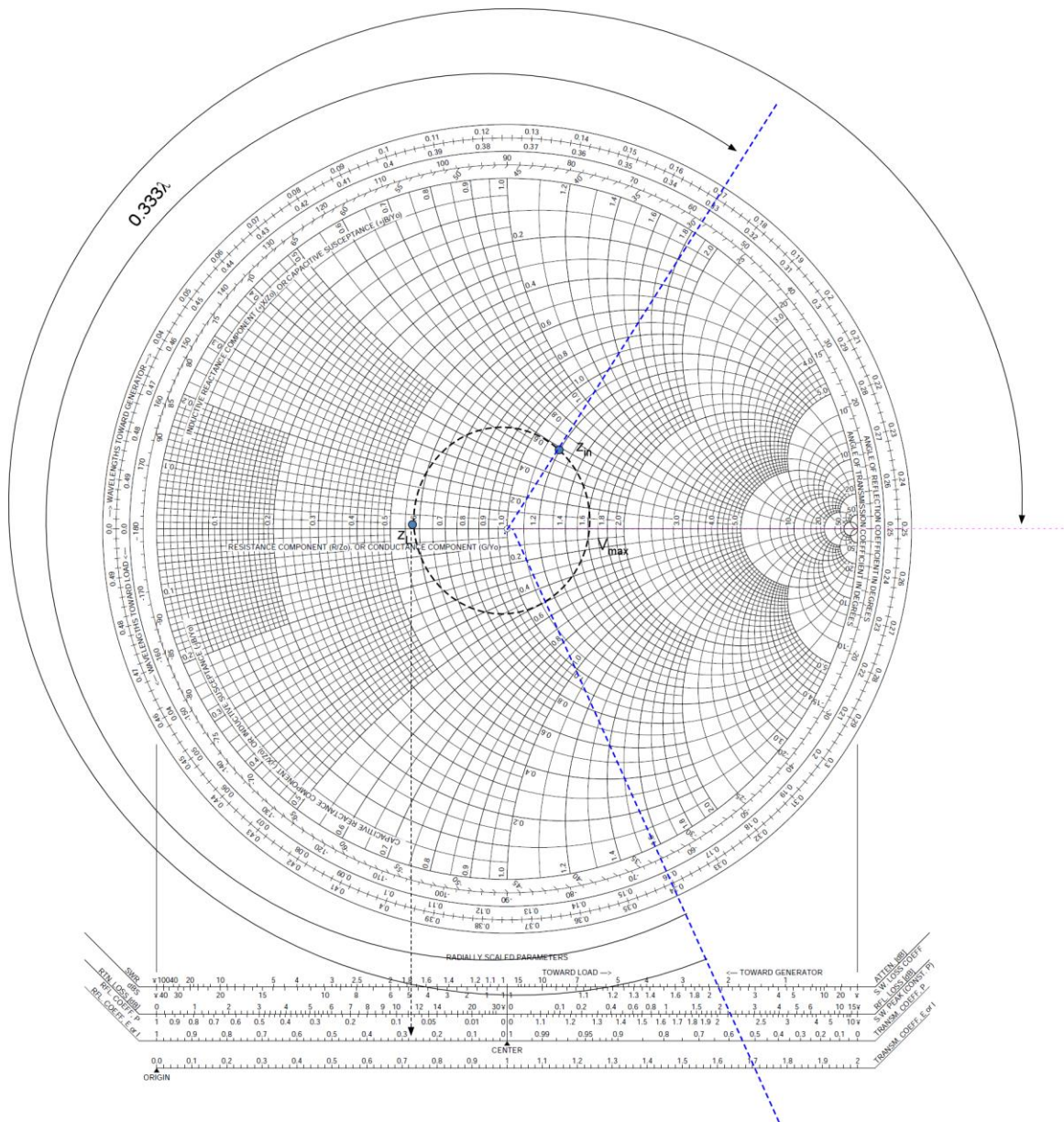
1. (10 points) On a lossless $50\text{-}\Omega$ transmission line terminated with a $Z_L = 100 + j100\ \Omega$. If this transmission line is to be matched to the load using a shorted load stub. Determine the stub length and distance between the load and stub. Two possible answers. You only need to show one of them.



2. (10 points) A 20-cm long air spaced lossless 50-Ω line ($\epsilon_r = 1$) is terminated in an unknown impedance. If the input impedance is $Z_{in} = 60 + j30\text{-}\Omega$ at frequency 5GHz, Find (1) the reflection coefficient; (2) the standing wave ratio (S) and (3) the location of the first voltage maximum from the load.

$$\lambda = \frac{c}{f} = \frac{3 \times 10^8 \text{ m/s}}{5 \times 10^9 \text{ Hz}} = 6 \text{ cm}. \quad z_{in} = \frac{Z_{in}}{Z_0} = 1.2 + j0.6$$

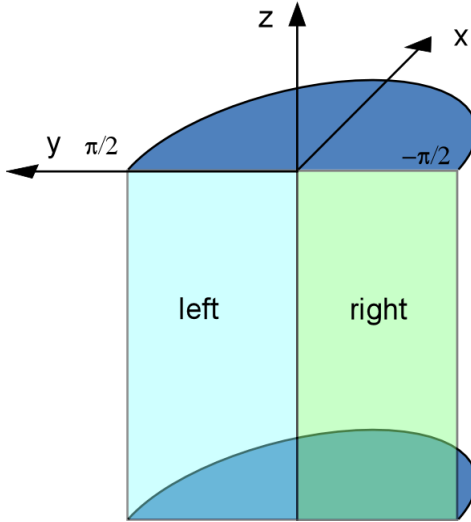
$$l = \frac{20 \text{ cm}}{6 \text{ cm}} = 3.333\lambda. \quad S = 1.7, \quad \Gamma = 0.3 \angle -68^\circ. \quad \text{Location at } 0.41\lambda \text{ from load.}$$



3. (10 points) For a vector field $\vec{A} = r^2 \hat{r} + 3r\phi \hat{\phi} - 2\hat{z}$, verify the divergence theorem

$$\oiint_s \vec{A} \cdot d\vec{s} = \iiint_v (\nabla \cdot \vec{A}) dv, \quad \text{on a section of a cylinder bounded by}$$

$$r=1, \quad -\frac{\pi}{2} \leq \phi \leq \frac{\pi}{2}, \quad 1 \leq z \leq 3.$$



Solution:

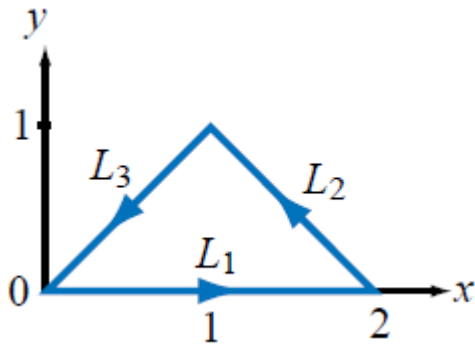
$$\begin{aligned} \oiint_s \vec{A} \cdot d\vec{s} &= \iint_{top} \vec{A} \cdot d\vec{s} + \iint_{bottom} \vec{A} \cdot d\vec{s} + \iint_{side} \vec{A} \cdot d\vec{s} + \iint_{left} \vec{A} \cdot d\vec{s} + \iint_{right} \vec{A} \cdot d\vec{s}, \\ \iint_{top} \vec{A} \cdot d\vec{s} &= \iint_{top} -2\hat{z} \cdot \hat{z} r dr d\phi = -\pi, \quad \iint_{bottom} \vec{A} \cdot d\vec{s} = \iint_{bottom} -2\hat{z} \cdot (-\hat{z}) r dr d\phi = \pi, \\ \iint_{side} \vec{A} \cdot d\vec{s} &= \iint_{side} r^2 \hat{r} \cdot \hat{r} r d\phi dz \Big|_{r=1} = 2\pi, \\ \iint_{left} \vec{A} \cdot d\vec{s} &= \iint_{left} 3r\phi \hat{\phi} \cdot \hat{\phi} r dz \Big|_{\phi=\pi/2} = \frac{3\pi}{2}, \\ \iint_{right} \vec{A} \cdot d\vec{s} &= \iint_{right} 3r\phi \hat{\phi} \cdot (-\hat{\phi}) r dz \Big|_{\phi=-\pi/2} = \frac{3\pi}{2}, \\ \oiint_s \vec{A} \cdot d\vec{s} &= \iint_{top} \vec{A} \cdot d\vec{s} + \iint_{bottom} \vec{A} \cdot d\vec{s} + \iint_{side} \vec{A} \cdot d\vec{s} + \iint_{left} \vec{A} \cdot d\vec{s} + \iint_{right} \vec{A} \cdot d\vec{s} = 5\pi. \end{aligned}$$

$$\nabla \cdot \vec{A} = \frac{1}{r} \frac{\partial}{\partial r} (r r^2) + \frac{1}{r} \frac{\partial}{\partial \phi} (3r\phi) = 3r + 3,$$

$$\iiint_v (\nabla \cdot \vec{A}) dv = \int_1^3 dz \int_{-\pi/2}^{\pi/2} d\phi \int_0^1 (3r + 3) r dr = 2\pi \left(r^3 + \frac{3}{2} r^2 \right) \Big|_0^1 = 5\pi,$$

$$\oiint_s \vec{A} \cdot d\vec{s} = \iiint_v (\nabla \cdot \vec{A}) dv.$$

4. (10 points) Verify Stokes's theorem for the vector field $\vec{A} = \hat{x}y^3 + \hat{y}x^3$ along the path shown below:



Solution:

$$\oint \vec{A} \cdot d\vec{l} = \int_{L_1} \vec{A} \cdot d\vec{l} + \int_{L_2} \vec{A} \cdot d\vec{l} + \int_{L_3} \vec{A} \cdot d\vec{l} .$$

$$\int_{L_1} \vec{A} \cdot d\vec{l} = \int_{L_1} (\hat{x}y^3 + \hat{y}x^3) \cdot \hat{x}dx \Big|_{y=0} = \int_{L_1} y^3 dx \Big|_{y=0} = 0 .$$

$$\int_{L_2} \vec{A} \cdot d\vec{l} = \int_2^1 (\hat{x}y^3 + \hat{y}x^3) \cdot \hat{x}dx \Big|_{y=2-x} + \int_0^1 (\hat{x}y^3 + \hat{y}x^3) \cdot \hat{y}dy \Big|_{x=2-y}$$

$$= \int_2^1 (2-x)^3 dx + \int_0^1 (2-y)^3 dy$$

$$= \int_1^2 (2-x)^3 d(2-x) - \int_0^1 (2-y)^3 d(2-y)$$

$$= \frac{1}{4} (2-x)^4 \Big|_1^2 - \frac{1}{4} (2-y)^4 \Big|_0^1$$

$$= -\frac{1}{4} - \frac{1}{4} (1-16) = \frac{14}{4}$$

$$\int_{L_3} \vec{A} \cdot d\vec{l} = \int_1^0 (\hat{x}y^3 + \hat{y}x^3) \cdot \hat{x}dx \Big|_{y=x} + \int_1^0 (\hat{x}y^3 + \hat{y}x^3) \cdot \hat{y}dy \Big|_{x=y}$$

$$= \int_1^0 x^3 dx + \int_1^0 y^3 dy$$

$$= -\frac{1}{4} x^4 \Big|_0^1 - \frac{1}{4} y^4 \Big|_0^1$$

$$= -\frac{2}{4}$$

$$\oint \vec{A} \cdot d\vec{l} = \int_{L_1} \vec{A} \cdot d\vec{l} + \int_{L_2} \vec{A} \cdot d\vec{l} + \int_{L_3} \vec{A} \cdot d\vec{l} = 0 + \frac{14}{4} - \frac{2}{4} = 3 .$$

$$\nabla \times \vec{A} = \begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ y^3 & x^3 & 0 \end{vmatrix} = \hat{x}0 + \hat{y}0 + \hat{z}(3x^2 - 3y^2)$$

$$\iint_s (\nabla \times \vec{A}) \cdot d\vec{s} = \iint_s \hat{z}(3x^2 - 3y^2) \cdot \hat{z} dx dy$$

$$= \int_0^1 dx \int_0^x (3x^2 - 3y^2) dy + \int_1^2 dx \int_0^{2-x} (3x^2 - 3y^2) dy$$

$$= \int_0^1 2x^3 dx + \int_1^2 [3x^2(2-x) - (2-x)^3] dx$$

$$= \frac{2}{4} + \int_1^2 3x^2(2-x) dx - \int_1^2 (2-x)^3 dx$$

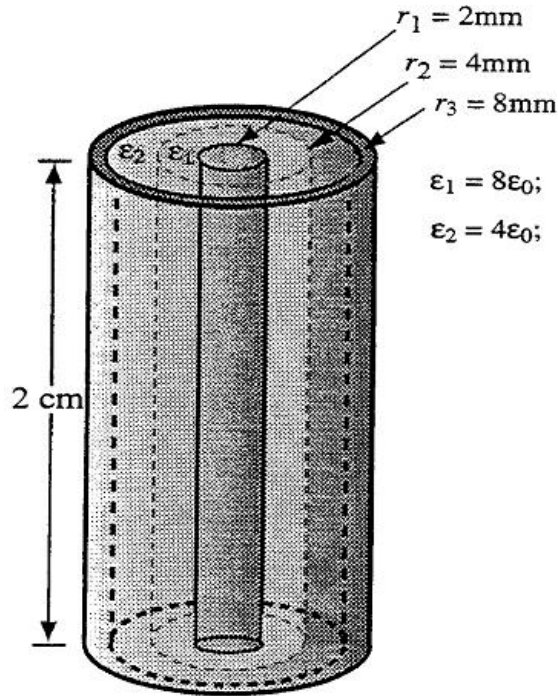
$$= \frac{2}{4} + 2x^3 \Big|_1^2 - \frac{3}{4} x^4 \Big|_1^2 + \frac{1}{4} (2-x)^4 \Big|_1^2$$

$$= \frac{2}{4} + 14 - \frac{3}{4} 15 - \frac{1}{4}$$

$$= 3$$

$$\oint \vec{A} \cdot d\vec{l} = \int_s (\nabla \times \vec{A}) \cdot d\vec{s}$$

5. (10 points) A coaxial capacitor with inner connector radius $r_1 = 2\text{mm}$, and outer connector radius $r_3 = 8\text{mm}$, is filled with two different materials as shown in the following figure. The length of the capacitor is 2cm . Calculate (1) if the surface charge density $\sigma = 1.0 \times 10^{-10} \text{C/cm}^2$, calculate the electric field inside the capacitor; (2) the capacitance of the capacitor. $\epsilon_0 = 8.85 \times 10^{-12} \text{F/m}$.



Solution:

Using Gauss's Law, the E fields are:

$$\vec{E} = \begin{cases} \frac{\sigma_1}{\epsilon_1 r}, & r_1 < r < r_2 \\ \frac{\sigma_1}{\epsilon_2 r}, & r_2 < r < r_3 \end{cases}$$

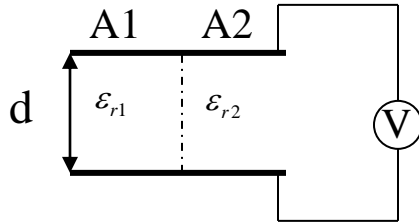
The voltage is:

$$V_{drop} = \int \vec{E} \cdot \hat{r} dr = \frac{\sigma_1}{\epsilon_1} \ln\left(\frac{r_2}{r_1}\right) + \frac{\sigma_1}{\epsilon_2} \ln\left(\frac{r_3}{r_2}\right),$$

$$Q = 2\pi r_1 L \sigma,$$

$$C = \frac{2\pi r_1 \sigma L}{\frac{\sigma_1}{\epsilon_1} \ln\left(\frac{r_2}{r_1}\right) + \frac{\sigma_1}{\epsilon_2} \ln\left(\frac{r_3}{r_2}\right)} = \frac{2\pi L}{\frac{1}{\epsilon_1} \ln\left(\frac{r_2}{r_1}\right) + \frac{1}{\epsilon_2} \ln\left(\frac{r_3}{r_2}\right)} = \frac{2\pi \epsilon_0 L}{\frac{1}{4} \ln\left(\frac{r_2}{r_1}\right) + \frac{1}{8} \ln\left(\frac{r_3}{r_2}\right)} = 4.3 \text{ pF}.$$

6. (10 points) A parallel-plate capacitor has two dielectric filling regions between the plate, $A_1 = 10\text{mm}^2$, $A_2 = 20\text{mm}^2$, $d = 5\text{mm}$, $V = 10\text{V}$, $\epsilon_{r1} = 1.5$, $\epsilon_{r2} = 3$, ignore fringing field effect. $\epsilon_0 = 8.85 \times 10^{-12} \text{ F/m}$.



Determine:

- Electric field E_1 , E_2 of the two regions.
- The capacitance of the capacitor.

Solution:

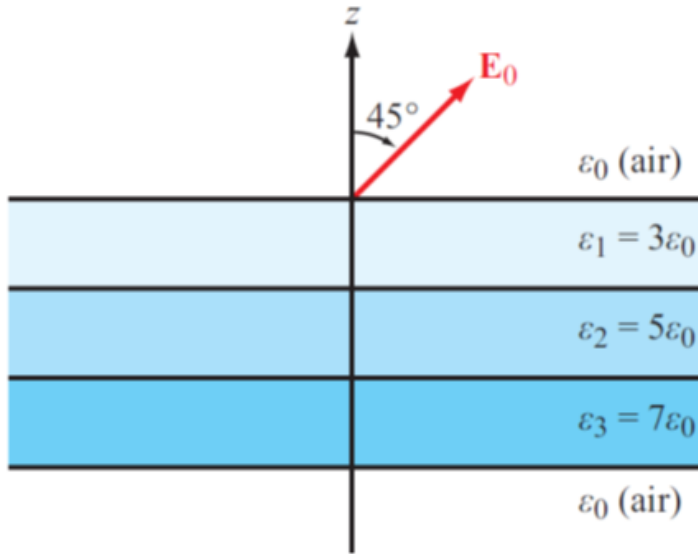
$$\vec{E}_1 = \vec{E}_2 = \frac{10\text{V}}{5\text{mm}} = 2 \times 10^3 (\text{V/m}),$$

$$\vec{D}_1 = \epsilon_1 \vec{E}_1, \vec{D}_2 = \epsilon_2 \vec{E}_2.$$

$$Q_1 = A_1 D_1, Q_2 = A_2 D_2$$

$$C = \frac{Q_1 + Q_2}{V} = \frac{\epsilon_1 E_1 A_1 + \epsilon_2 E_2 A_2}{E_1 d} = \epsilon_0 \frac{1.5 \cdot 10\text{mm}^2 + 3 \cdot 20\text{mm}^2}{5\text{mm}} = 0.13\text{pF}.$$

7. (10 points) Determine the electric field intensity vectors in each layer.



Solutions:

Layer ϵ_1 :

$$E_{1t} = E_{0t} = \frac{\sqrt{2}}{2} E_0, \quad \epsilon_1 E_{1z} = \epsilon_0 E_{0z}, \quad E_{1z} = \frac{\epsilon_0}{\epsilon_1} E_{0z} = \frac{\sqrt{2}}{6} E_0,$$

Layer ϵ_2 :

$$E_{2t} = E_{1t} = \frac{\sqrt{2}}{2} E_0, \quad \epsilon_2 E_{2z} = \epsilon_1 E_{1z} = \epsilon_0 E_{0z}, \quad E_{2z} = \frac{\epsilon_0}{\epsilon_2} E_{0z} = \frac{\sqrt{2}}{10} E_0,$$

Layer ϵ_3 :

$$E_{3t} = E_{2t} = \frac{\sqrt{2}}{2} E_0, \quad \epsilon_3 E_{3z} = \epsilon_2 E_{2z} = \epsilon_0 E_{0z}, \quad E_{3z} = \frac{\epsilon_0}{\epsilon_3} E_{0z} = \frac{\sqrt{2}}{14} E_0,$$

Layer ϵ_0 :

$$E_{4t} = E_{3t} = \frac{\sqrt{2}}{2} E_0, \quad \epsilon_0 E_{4z} = \epsilon_3 E_{3z} = \epsilon_0 E_{0z}, \quad E_{4z} = \frac{\epsilon_0}{\epsilon_0} E_{0z} = \frac{\sqrt{2}}{2} E_0.$$

8. (10 points) If the inner conductor of a coaxial cable carries a current of I , calculate the magnetic field inside the coaxial cable. The inner radius of the coaxial cable is r_1 , and the outer radius is r_2 . Assuming the permeability of material inside the coaxial cable is μ_0 .

Solution:

Applying Ampere's law:

$$\oint \vec{H} \cdot d\vec{l} = I, \quad H(r)2\pi r = I,$$

$$H(r) = \frac{I}{2\pi r}, \quad r_1 < r < r_2$$

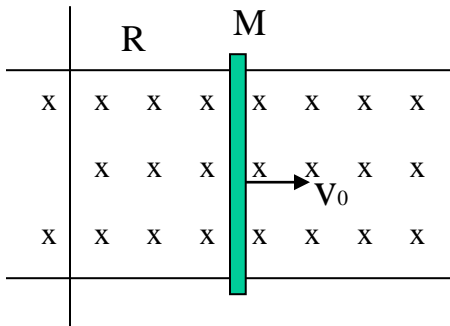
$$\vec{H} = \hat{\phi} \frac{I}{2\pi r}, \quad r_1 < r < r_2$$

$$\vec{B} = \mu_0 \vec{H} = \hat{\phi} \frac{I\mu_0}{2\pi r}, \quad r_1 < r < r_2$$

9. (10 points) Write down the Maxwell equations and their integral forms.

10. (10 points) A conducting bar is put in a constant magnetic field $B = 0.1\text{T}$. The circuit resistance is $R = 10\Omega$. The bar width is 20cm . The mass of the bar is $m = 1\text{kg}$. The circuit and the metal bar are on a flat horizontal surface. If the bar has an initial speed ($t = 0$) of $V_0 = 4\text{m/s}$, determine:

- (1) the current generated in the bar at $t = 0$;
- (2) the force experienced by the conducting bar at $t = 0$;
- (3) the speed of the bar at time $t = 10\text{s}$;
- (4) the current generated at $t = 10\text{s}$?
- (5) (extra 5 points) prove that the kinetic energy loss of the metal bar is converted to the resistor heating power with a 100% energy conversion efficiency.



$$(1) V = -\frac{\partial}{\partial t}(B \cdot W \cdot L(t)) = BWv_0$$

$$I = \frac{V}{R} = \frac{BWv_0}{R} = 8(\text{mA}), \text{ counter clockwise}$$

$$(2) F = BWI = 1.6 \times 10^{-4} \text{ (N)}, \text{ pointing to the left.}$$

$$(3) F = -m \frac{d}{dt} v = \frac{B^2 W^2}{R} v,$$

$$v = v_0 e^{-\frac{W^2 B^2}{mR} t}$$

$$(4) I = \frac{WBv_0}{R} e^{-\frac{W^2 B^2}{mR} t}$$

Voltage maximum	$ \tilde{V} _{\max} = V_0^+ [1 + \Gamma]$
Voltage minimum	$ \tilde{V} _{\min} = V_0^+ [1 - \Gamma]$
Positions of voltage maxima (also positions of current minima)	$l_{\max} = \frac{\theta_r \lambda}{4\pi} + \frac{n\lambda}{2}, \quad n = 0, 1, 2, \dots$
Position of first maximum (also position of first current minimum)	$l_{\max} = \begin{cases} \frac{\theta_r \lambda}{4\pi}, & \text{if } 0 \leq \theta_r \leq \pi \\ \frac{\theta_r \lambda}{4\pi} + \frac{\lambda}{2}, & \text{if } -\pi \leq \theta_r \leq 0 \end{cases}$
Positions of voltage minima (also positions of first current maxima)	$l_{\min} = \frac{\theta_r \lambda}{4\pi} + \frac{(2n+1)\lambda}{4}, \quad n = 0, 1, 2, \dots$
Position of first minimum (also position of first current maximum)	$l_{\min} = \frac{\lambda}{4} \left(1 + \frac{\theta_r}{\pi} \right)$
Input impedance	$Z_{\text{in}} = Z_0 \left(\frac{Z_L + jZ_0 \tan \beta l}{Z_0 + jZ_L \tan \beta l} \right)$
Positions at which Z_{in} is real	at voltage maxima and minima
Z_{in} at voltage maxima	$Z_{\text{in}} = Z_0 \left(\frac{1 + \Gamma }{1 - \Gamma } \right)$
Z_{in} at voltage minima	$Z_{\text{in}} = Z_0 \left(\frac{1 - \Gamma }{1 + \Gamma } \right)$
Z_{in} of short-circuited line	$Z_{\text{in}}^{\text{sc}} = jZ_0 \tan \beta l$
Z_{in} of open-circuited line	$Z_{\text{in}}^{\text{oc}} = -jZ_0 \cot \beta l$
Z_{in} of line of length $l = n\lambda/2$	$Z_{\text{in}} = Z_L, \quad n = 0, 1, 2, \dots$
Z_{in} of line of length $l = \lambda/4 + n\lambda/2$	$Z_{\text{in}} = Z_0^2/Z_L, \quad n = 0, 1, 2, \dots$
Z_{in} of matched line	$Z_{\text{in}} = Z_0$
$ V_0^+ $ = amplitude of incident wave, $\Gamma = \Gamma e^{j\theta_r}$ with $-\pi < \theta_r < \pi$; θ_r in radians.	

$$\Gamma = \frac{Z_L - Z_0}{Z_L + Z_0}$$

$$S = \frac{1 + |\Gamma|}{1 - |\Gamma|}$$

GRADIENT, DIVERGENCE, CURL, & LAPLACIAN OPERATORS

CARTESIAN (RECTANGULAR) COORDINATES (x, y, z)

$$\nabla V = x \frac{\partial V}{\partial x} + y \frac{\partial V}{\partial y} + z \frac{\partial V}{\partial z}$$

$$\nabla \cdot \mathbf{A} = \frac{\partial A_x}{\partial x} + \frac{\partial A_y}{\partial y} + \frac{\partial A_z}{\partial z}$$

$$\nabla \times \mathbf{A} = \begin{vmatrix} \mathbf{x} & \mathbf{y} & \mathbf{z} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ A_x & A_y & A_z \end{vmatrix} = \mathbf{x} \left(\frac{\partial A_z}{\partial y} - \frac{\partial A_y}{\partial z} \right) + \mathbf{y} \left(\frac{\partial A_x}{\partial z} - \frac{\partial A_z}{\partial x} \right) + \mathbf{z} \left(\frac{\partial A_y}{\partial x} - \frac{\partial A_x}{\partial y} \right)$$

$$\nabla^2 V = \frac{\partial^2 V}{\partial x^2} + \frac{\partial^2 V}{\partial y^2} + \frac{\partial^2 V}{\partial z^2}$$

CYLINDRICAL COORDINATES (r, ϕ, z)

$$\nabla V = \mathbf{r} \frac{\partial V}{\partial r} + \phi \frac{1}{r} \frac{\partial V}{\partial \phi} + \mathbf{z} \frac{\partial V}{\partial z}$$

$$\nabla \cdot \mathbf{A} = \frac{1}{r} \frac{\partial}{\partial r} (rA_r) + \frac{1}{r} \frac{\partial A_\phi}{\partial \phi} + \frac{\partial A_z}{\partial z}$$

$$\nabla \times \mathbf{A} = \frac{1}{r} \begin{vmatrix} \mathbf{r} & \phi \mathbf{r} & \mathbf{z} \\ \frac{\partial}{\partial r} & \frac{\partial}{\partial \phi} & \frac{\partial}{\partial z} \\ A_r & rA_\phi & A_z \end{vmatrix} = \mathbf{r} \left(\frac{1}{r} \frac{\partial A_z}{\partial \phi} - \frac{\partial A_\phi}{\partial z} \right) + \phi \left(\frac{\partial A_r}{\partial z} - \frac{\partial A_z}{\partial r} \right) + \mathbf{z} \frac{1}{r} \left[\frac{\partial}{\partial r} (rA_\phi) - \frac{\partial A_r}{\partial \phi} \right]$$

$$\nabla^2 V = \frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial V}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2 V}{\partial \phi^2} + \frac{\partial^2 V}{\partial z^2}$$

SPHERICAL COORDINATES (R, θ, ϕ)

$$\nabla V = \mathbf{R} \frac{\partial V}{\partial R} + \theta \frac{1}{R} \frac{\partial V}{\partial \theta} + \phi \frac{1}{R \sin \theta} \frac{\partial V}{\partial \phi}$$

$$\nabla \cdot \mathbf{A} = \frac{1}{R^2} \frac{\partial}{\partial R} (R^2 A_R) + \frac{1}{R \sin \theta} \frac{\partial}{\partial \theta} (A_\theta \sin \theta) + \frac{1}{R \sin \theta} \frac{\partial A_\phi}{\partial \phi}$$

$$\nabla \times \mathbf{A} = \frac{1}{R^2 \sin \theta} \begin{vmatrix} \mathbf{R} & \theta \mathbf{R} & \phi R \sin \theta \\ \frac{\partial}{\partial R} & \frac{\partial}{\partial \theta} & \frac{\partial}{\partial \phi} \\ A_R & R A_\theta & (R \sin \theta) A_\phi \end{vmatrix}$$

$$= \mathbf{R} \frac{1}{R \sin \theta} \left[\frac{\partial}{\partial \theta} (A_\phi \sin \theta) - \frac{\partial A_\theta}{\partial \phi} \right] + \theta \frac{1}{R} \left[\frac{1}{\sin \theta} \frac{\partial A_R}{\partial \phi} - \frac{\partial}{\partial R} (R A_\phi) \right] + \phi \frac{1}{R} \left[\frac{\partial}{\partial R} (R A_\theta) - \frac{\partial A_R}{\partial \theta} \right]$$

$$\nabla^2 V = \frac{1}{R^2} \frac{\partial}{\partial R} \left(R^2 \frac{\partial V}{\partial R} \right) + \frac{1}{R^2 \sin \theta} \frac{\partial}{\partial \theta} \left(\sin \theta \frac{\partial V}{\partial \theta} \right) + \frac{1}{R^2 \sin^2 \theta} \frac{\partial^2 V}{\partial \phi^2}$$

Table 3-1: Summary of vector relations.

	Cartesian Coordinates	Cylindrical Coordinates	Spherical Coordinates
Coordinate variables	x, y, z	r, ϕ, z	R, θ, ϕ
Vector representation, $\mathbf{A} =$	$\hat{x}A_x + \hat{y}A_y + \hat{z}A_z$	$\hat{r}A_r + \hat{\phi}A_\phi + \hat{z}A_z$	$\hat{\mathbf{R}}A_R + \hat{\theta}A_\theta + \hat{\phi}A_\phi$
Magnitude of \mathbf{A} , $ \mathbf{A} =$	$\sqrt{A_x^2 + A_y^2 + A_z^2}$	$\sqrt{A_r^2 + A_\phi^2 + A_z^2}$	$\sqrt{A_R^2 + A_\theta^2 + A_\phi^2}$
Position vector $\overrightarrow{OP_1} =$	$\hat{x}x_1 + \hat{y}y_1 + \hat{z}z_1,$ for $P(x_1, y_1, z_1)$	$\hat{r}r_1 + \hat{z}z_1,$ for $P(r_1, \phi_1, z_1)$	$\hat{\mathbf{R}}R_1,$ for $P(R_1, \theta_1, \phi_1)$
Base vectors properties	$\hat{x} \cdot \hat{x} = \hat{y} \cdot \hat{y} = \hat{z} \cdot \hat{z} = 1$ $\hat{x} \cdot \hat{y} = \hat{y} \cdot \hat{z} = \hat{z} \cdot \hat{x} = 0$ $\hat{x} \times \hat{y} = \hat{z}$ $\hat{y} \times \hat{z} = \hat{x}$ $\hat{z} \times \hat{x} = \hat{y}$	$\hat{r} \cdot \hat{r} = \hat{\phi} \cdot \hat{\phi} = \hat{z} \cdot \hat{z} = 1$ $\hat{r} \cdot \hat{\phi} = \hat{\phi} \cdot \hat{z} = \hat{z} \cdot \hat{r} = 0$ $\hat{r} \times \hat{\phi} = \hat{z}$ $\hat{\phi} \times \hat{z} = \hat{r}$ $\hat{z} \times \hat{r} = \hat{\phi}$	$\hat{\mathbf{R}} \cdot \hat{\mathbf{R}} = \hat{\theta} \cdot \hat{\theta} = \hat{\phi} \cdot \hat{\phi} = 1$ $\hat{\mathbf{R}} \cdot \hat{\theta} = \hat{\theta} \cdot \hat{\phi} = \hat{\phi} \cdot \hat{\mathbf{R}} = 0$ $\hat{\mathbf{R}} \times \hat{\theta} = \hat{\phi}$ $\hat{\theta} \times \hat{\phi} = \hat{\mathbf{R}}$ $\hat{\phi} \times \hat{\mathbf{R}} = \hat{\theta}$
Dot product, $\mathbf{A} \cdot \mathbf{B} =$	$A_x B_x + A_y B_y + A_z B_z$	$A_r B_r + A_\phi B_\phi + A_z B_z$	$A_R B_R + A_\theta B_\theta + A_\phi B_\phi$
Cross product, $\mathbf{A} \times \mathbf{B} =$	$\begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ A_x & A_y & A_z \\ B_x & B_y & B_z \end{vmatrix}$	$\begin{vmatrix} \hat{r} & \hat{\phi} & \hat{z} \\ A_r & A_\phi & A_z \\ B_r & B_\phi & B_z \end{vmatrix}$	$\begin{vmatrix} \hat{\mathbf{R}} & \hat{\theta} & \hat{\phi} \\ A_R & A_\theta & A_\phi \\ B_R & B_\theta & B_\phi \end{vmatrix}$
Differential length, $d\mathbf{l} =$	$\hat{x} dx + \hat{y} dy + \hat{z} dz$	$\hat{r} dr + \hat{\phi} r d\phi + \hat{z} dz$	$\hat{\mathbf{R}} dR + \hat{\theta} R d\theta + \hat{\phi} R \sin\theta d\phi$
Differential surface areas	$ds_x = \hat{x} dy dz$ $ds_y = \hat{y} dx dz$ $ds_z = \hat{z} dx dy$	$ds_r = \hat{r} r d\phi dz$ $ds_\phi = \hat{\phi} dr dz$ $ds_z = \hat{z} r dr d\phi$	$ds_R = \hat{\mathbf{R}} R^2 \sin\theta d\theta d\phi$ $ds_\theta = \hat{\theta} R \sin\theta dR d\phi$ $ds_\phi = \hat{\phi} R dR d\theta$
Differential volume, $dV =$	$dx dy dz$	$r dr d\phi dz$	$R^2 \sin\theta dR d\theta d\phi$

Boundary conditions:

$$D_{1n} - D_{2n} = \rho_s$$

$$H_{1x} - H_{2x} = J_y$$

$$H_{1y} - H_{2y} = -J_x$$