

Topics:

- Introduction to Optical Amplifier – types and applications
- Erbium-doped fiber amplifier (EDFA)
- External pumping and amplifier gain
- Power-conversion efficiency and gain profile

## Some basic concepts

- Power in dBm

$$P(\text{dBm}) = 10 \log \left[ \frac{P(\text{mW})}{1(\text{mW})} \right],$$

- Examples:

$$P = 1(\text{mW}) = 10 \log \left[ \frac{P(\text{mW})}{1(\text{mW})} \right] (\text{dBm}) = 0(\text{dBm}),$$

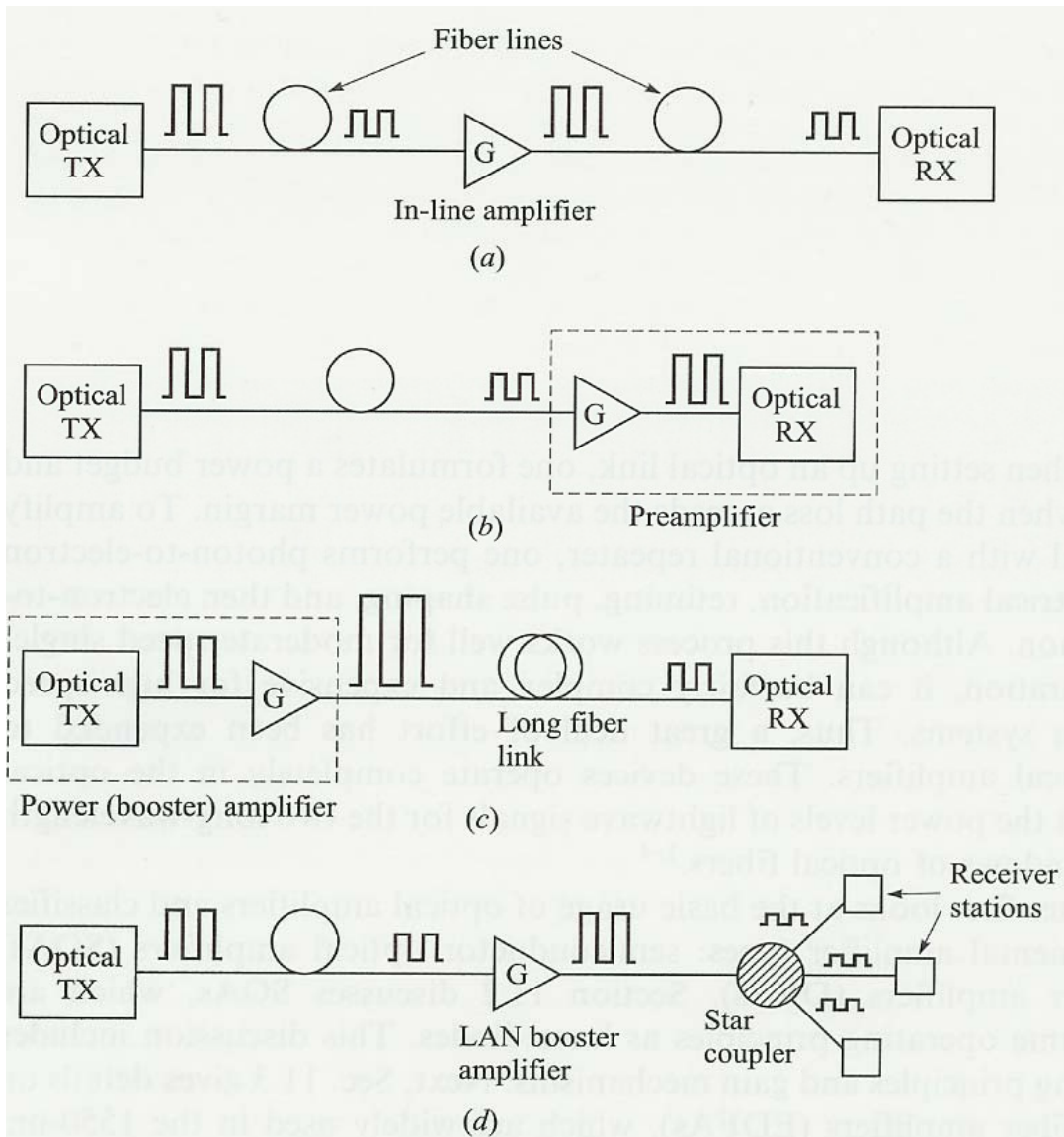
$$P = 2(\text{mW}) = 3(\text{dBm}), \quad P = 10(\text{mW}) = 10(\text{dBm}), \quad P = 1(\mu\text{W}) = -30(\text{dBm}),$$

- Noise figure (NF): SNR degradation

$$NF|_{\text{linear}} = \frac{(S/N)_{\text{input}}}{(S/N)_{\text{output}}},$$

$$NF|_{\text{dB}} = 10 \log \frac{(S/N)_{\text{input}}}{(S/N)_{\text{output}}} = 10 \log(S/N)_{\text{input}} - 10 \log(S/N)_{\text{output}},$$

## Introduction to optical amplifier

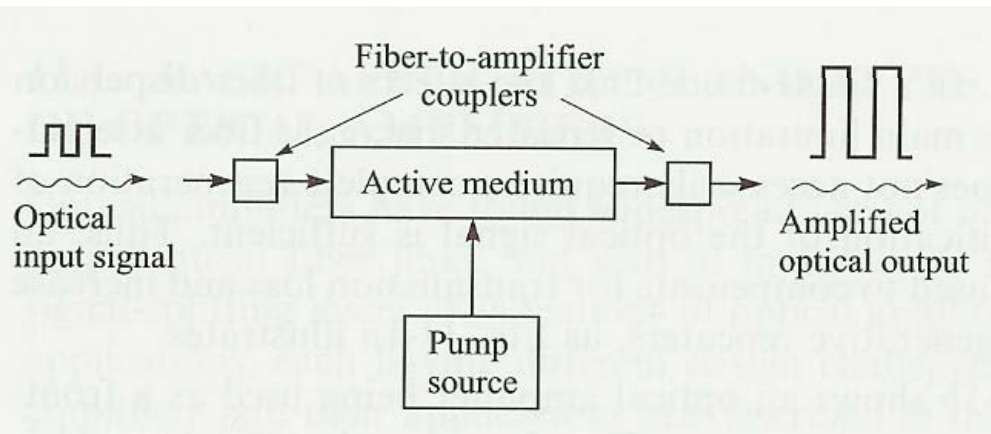


## Applications:

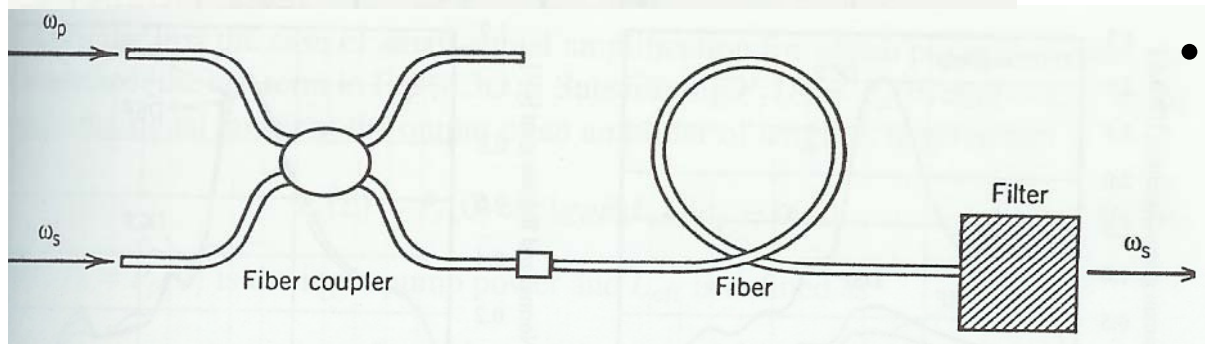
- **in-line amplifier**
  - input  $-25$  to  $-20$  dBm
  - output  $\sim 0$  to  $5$  dBm
  - Gain  $\sim 20$  dB
  - Noise figure  $< 4$  dB
- **Preamplifier**
  - input  $-35$  to  $-30$  dBm
  - output  $\sim -15$  to  $-10$  dBm
  - Gain  $\sim 20$  dB, Noise figure  $< 5$  dB
- **Power (booster) amplifier**
  - input  $-5$  to  $0$  dBm
  - output  $\sim 10$  to  $20$  dBm
  - Gain  $\sim 15$  dB, Noise figure  $< 4$  dB
- **LAN-booster**
  - input  $-25$  to  $-20$  dBm
  - output  $\sim 5$  to  $15$  dBm
  - Gain  $\sim 30$  dB, Noise figure  $< 4$  dB

## Types of Optical Amplifiers

- Erbium doped fiber amplifier
- Raman amplifier
- Semiconductor amplifier



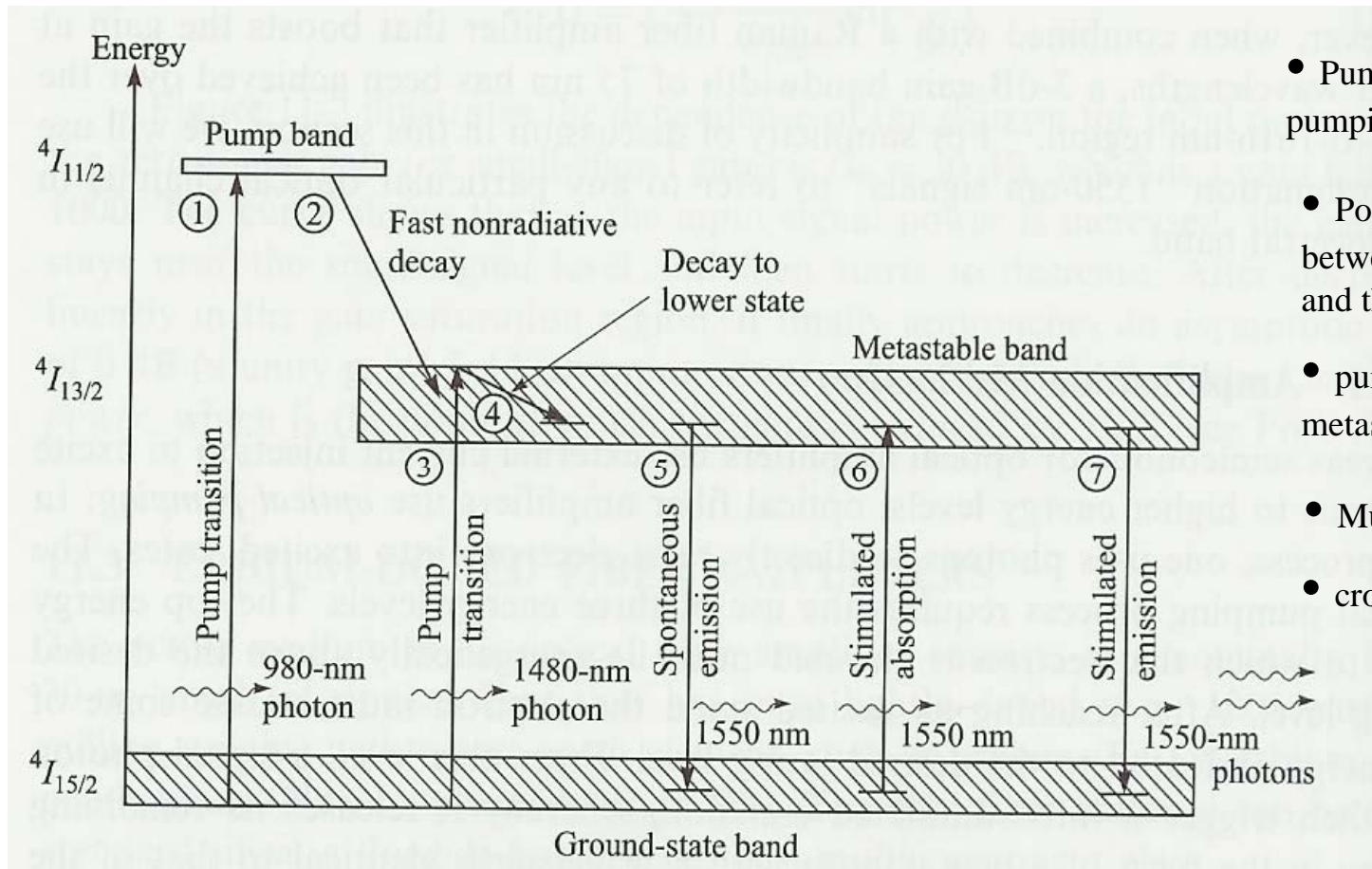
- Erbium doped fiber amplifier  
Active gain medium needed



- Raman amplifier  
Fiber nonlinearity  
Filter needed

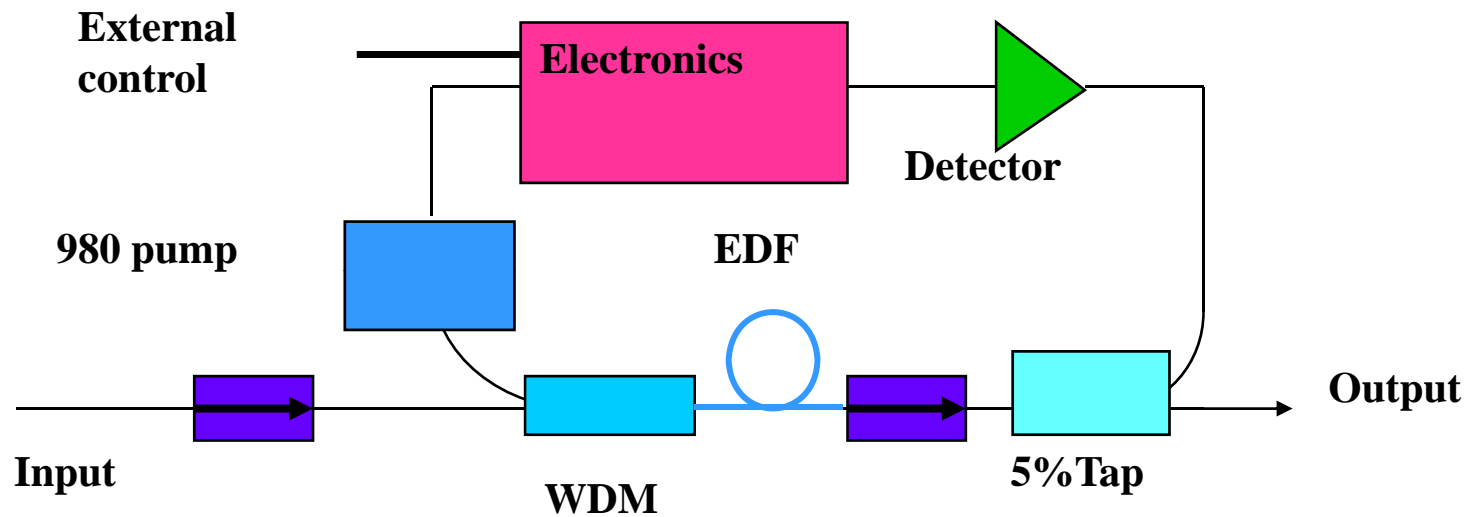
## Erbium doped fiber amplifier

- Optical pumping, 980nm or 1480nm laser



- Pump band is narrow, so the pumping laser has to be narrow
- Population inversion between the metastable band and the ground band
- pump band lifetime  $\sim 1\mu\text{s}$   
metastable lifetime  $\sim 10\text{ms}$ .
- Multi-channel amplification
- cross-talk issues

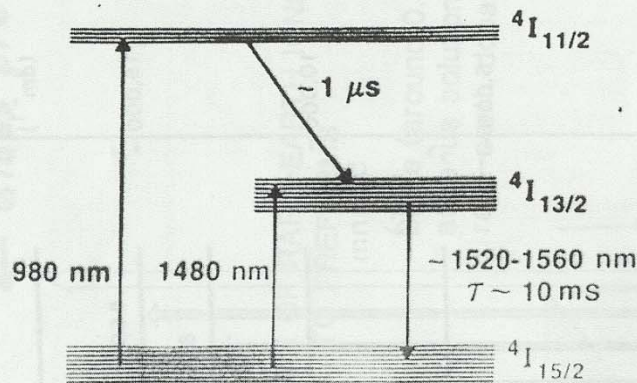
## Amplifier architecture



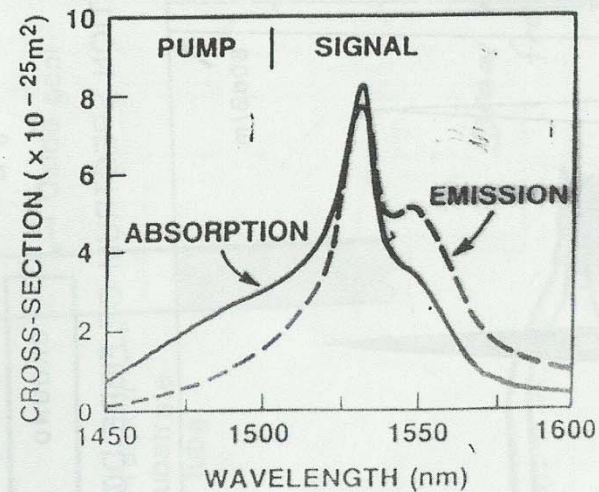


# Er-doped Glass Pump Bands

ENERGY LEVEL DIAGRAM



ABSORPTION AND EMISSION SPECTRA

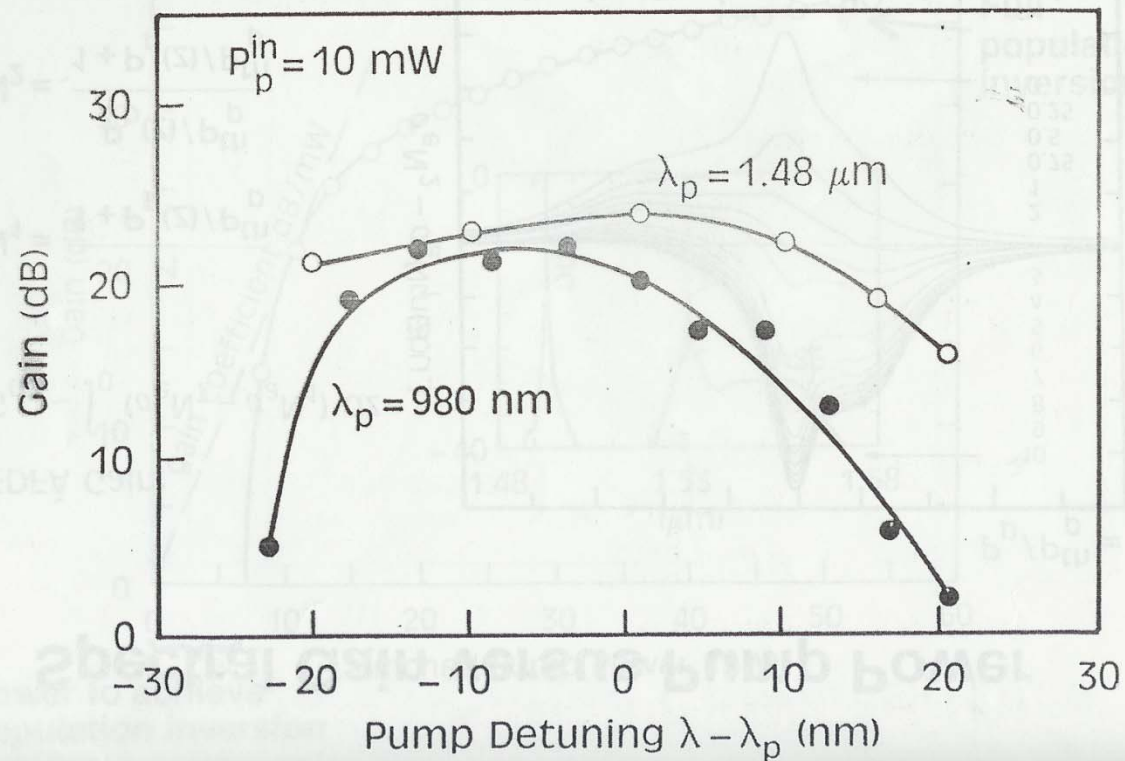


Pump/signal  $\lambda$ MUX  
 Pump efficiency  
 Spectral gain  
 Noise figure

980 (nm)  
 Easy  
 4 dB/mW  
 Peaky  
 ~ 3 dB

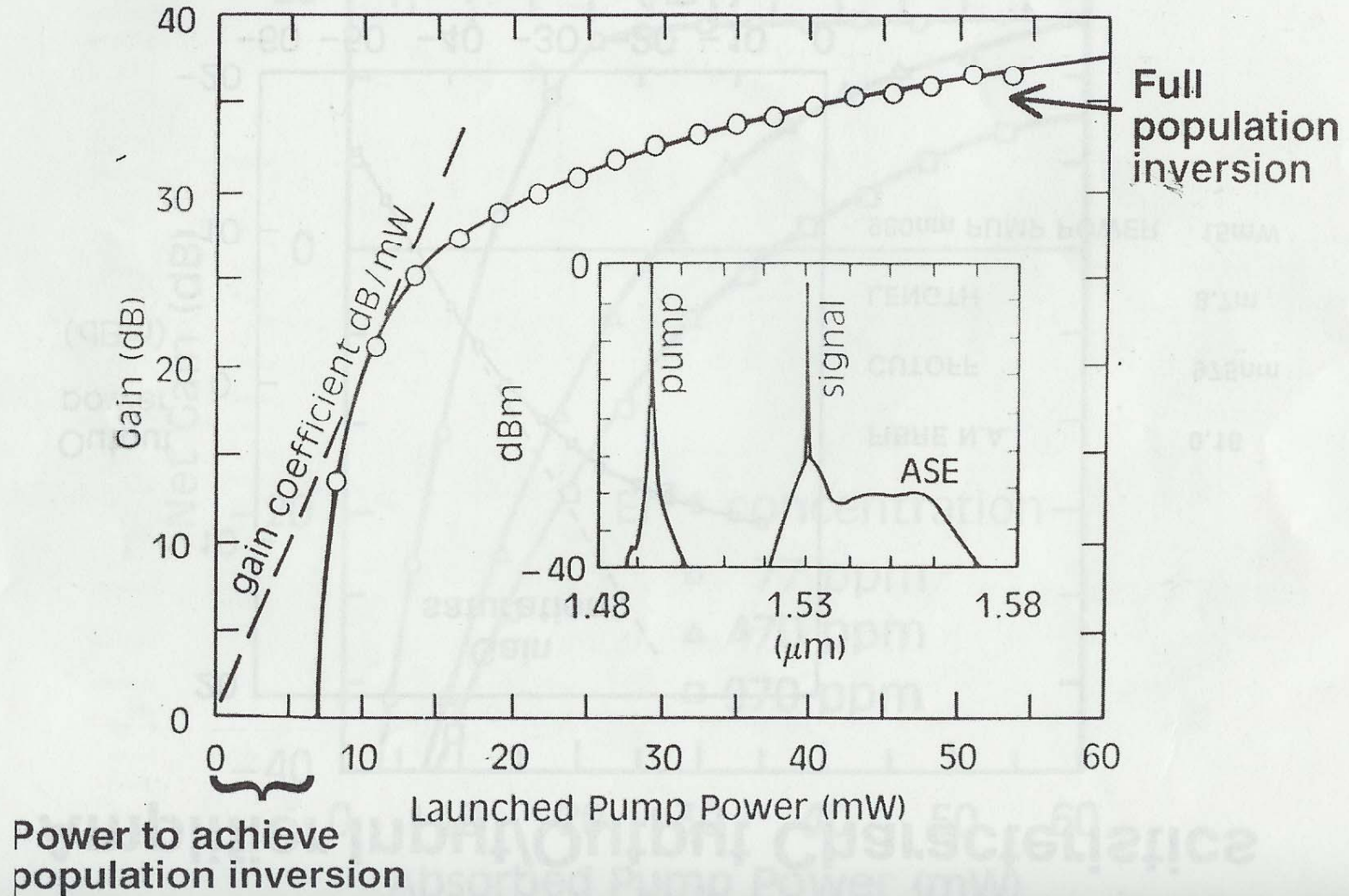
1490 (nm)  
 Difficult  
 2 dB/mW  
 Smoother  
 ~ 5 dB

## Spectral Gain Dependence on Pump Wavelength





# Optical Gain versus Pump Power



# Spectral Gain versus Pump Power

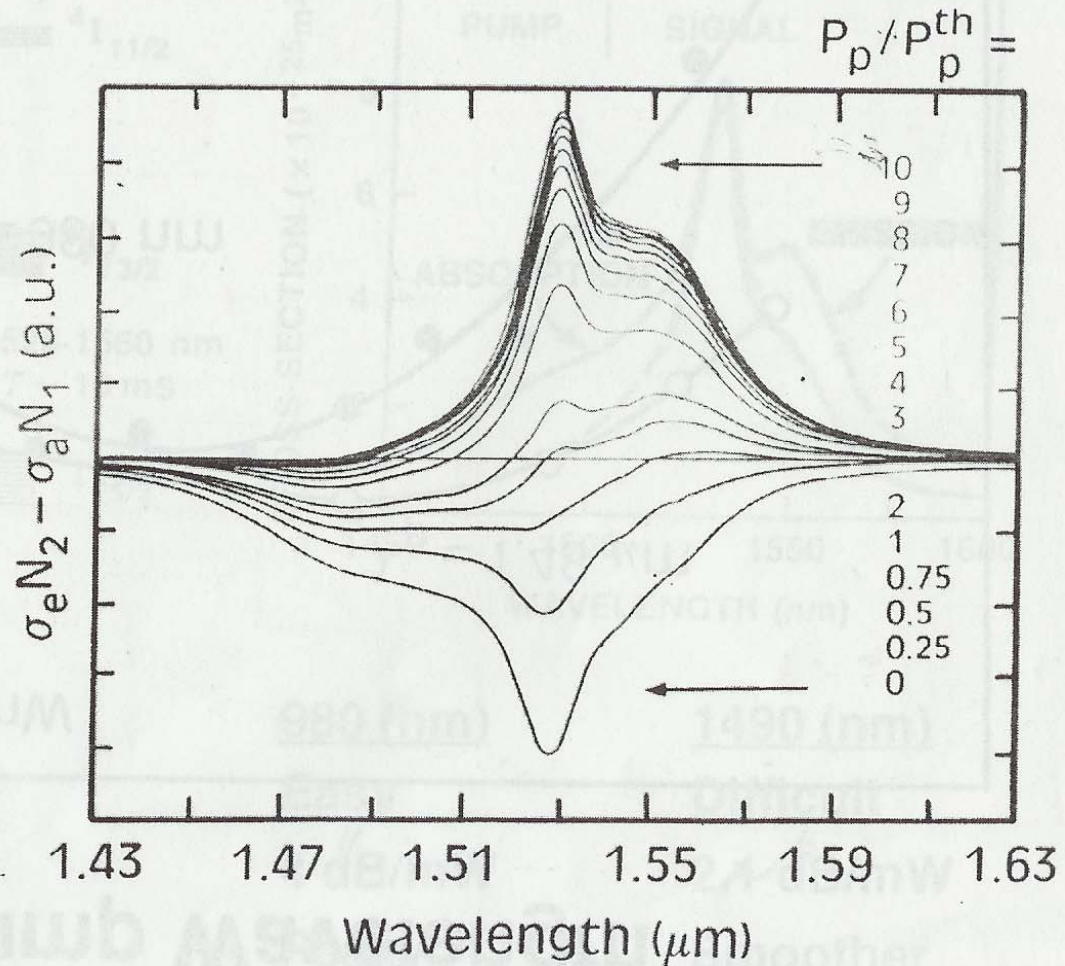
EDFA Gain:

$$G_{\text{dB}} \sim \int_0^L (\sigma_e N_2 - \sigma_a N_1) dz$$

$$N_1 = \frac{1}{1 + P_p(z)/P_p^{\text{th}}}$$

$$N_2 = \frac{P_p(z)/P_p^{\text{th}}}{1 + P_p(z)/P_p^{\text{th}}}$$

(3-level system)



## Power conversion efficiency

$$P_{s,out} \leq P_{s,in} + \frac{\lambda_p}{\lambda_s} P_{p,in},$$

$$PCE = \frac{P_{s,out} - P_{s,in}}{P_{p,in}} \approx \frac{P_{s,out}}{P_{s,in}} \leq \frac{\lambda_p}{\lambda_s},$$

$$P_{s,in} \leq \frac{(\lambda_p / \lambda_s) P_{p,in}}{G - 1},$$

Consider an EDFA being pumped at 980nm with a 30-mW pump. If the gain at 1550nm is 20dB, then what's the maximum input power?

$$P_{s,in} \leq \frac{(\lambda_p / \lambda_s) P_{p,in}}{G - 1} = 190 \mu\text{W} = -7.2 \text{dBm},$$

## Einstein's A and B coefficients

Assuming a two-level system:



Spontaneous emission rate:

$$R_{sp} = A_{21}N_2,$$

Stimulated emission rate:

$$R_{st} = B_{21}N_2P(h\nu),$$

Absorption rate:

$$R_{ab} = B_{12}N_1P(h\nu),$$

Steady state:

$$R_{sb} = R_{st} + R_{sp}$$

$$A_{21}N_2 + B_{21}N_2P(h\nu) = B_{12}N_1P(h\nu)$$

$$A_{21}N_2 = B_{12}N_1P(h\nu) - B_{21}N_2P(h\nu)$$

## Einstein's A and B coefficients

Assuming a two-level system:

$$\begin{array}{c}
 2 \text{ ————— } N_2 \\
 \\
 1 \text{ ————— } N_1
 \end{array}
 \quad
 A_{21}N_1 e^{-\frac{E_2-E_1}{kT}} = N_2 P(h\nu) d\nu \left( B_{12} e^{\frac{E_2-E_1}{kT}} - B_{21} \right)$$

$$P(h\nu) d\nu = \frac{8\pi h \nu^3}{c^3} \frac{d\nu}{e^{\hbar\omega/kT} - 1}$$

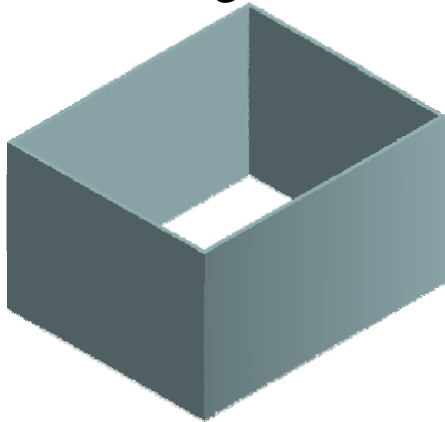
$$A_{21}N_1 e^{-\frac{E_2-E_1}{kT}} = N_1 e^{-\frac{E_2-E_1}{kT}} \frac{8\pi \nu^3}{c^3} \frac{d\nu}{e^{\hbar\omega/kT} - 1} \left( B_{12} e^{\frac{E_2-E_1}{kT}} - B_{21} \right)$$

$$B_{21} = B_{12}$$

$$A_{21} = B_{12} \frac{8\pi h \nu^3}{c^3} d\nu$$

## Photon energy density

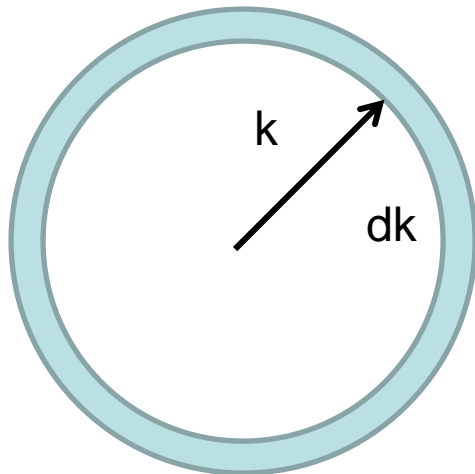
Assuming a blackbody cavity:



$$L_x \quad L_y \quad L_z \quad \sin k_m L_x = 0 \quad k_m = \pm \frac{m\pi}{L_x}$$

Volume of each mode at k-space

$$\frac{2\pi}{L_x} \frac{2\pi}{L_y} \frac{2\pi}{L_z}$$



Volume between k to k+dk

$$2 \times 4\pi k^2 dk$$

# of modes between k to k+dk

$$\frac{8\pi k^2 dk}{\left( \frac{2\pi}{L_x} \frac{2\pi}{L_y} \frac{2\pi}{L_z} \right)} = \frac{8\pi k^2 dk}{(2\pi)^3} V$$



## Photon energy density

# of modes between  $k$  to  $k+dk$  per volume

$$\frac{8\pi k^2 dk}{(2\pi)^3}$$

E and k relation  $k = \frac{2\pi}{\lambda} = \frac{2\pi\nu}{c}$

# of modes between  $\nu$  to  $\nu+d\nu$  per volume

$$\frac{8\pi}{(2\pi)^3} \left( \frac{2\pi\nu}{c} \right)^2 \frac{2\pi}{c} d\nu = \frac{8\pi\nu^2}{c^3} d\nu$$

Photon energy density for  $h\nu$ :

$$\left( \frac{8\pi\nu^2}{c^3} d\nu \right) h\nu \times N_{\text{photon/mode}} = \frac{8\pi h\nu^3}{c^3} \frac{d\nu}{e^{h\nu/kT} - 1}$$

$$P(h\nu)d\nu = \frac{8\pi h\nu^3}{c^3} \frac{d\nu}{e^{h\nu/kT} - 1}$$

Photon energy density

$$P(h\nu)d\nu = \frac{8\pi h\nu^3}{c^3} \frac{d\nu}{e^{h\nu/kT} - 1}$$

For blackbody

$$B_{21} = B_{12}$$

$$A_{21} = B_{12} \frac{8\pi h\nu^3}{c^3} d\nu$$

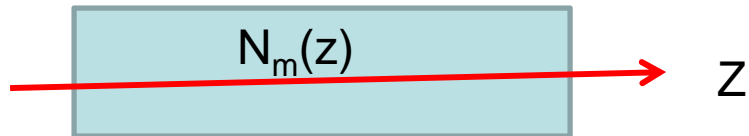
Einstein's A and B coefficients for Blackbody

$$B_{21} = B_{12}$$

$$A_{21} = B_{12} N_{\text{mode}} h\nu$$

Einstein's A and B coefficients for general cases

For a two-level amplifier



$$\frac{dN_m}{dz} = (N_2 - N_1)P_m(h\nu)dvB_{21} + A_{21}N_2 |_{N_m},$$

$$A_{21} = N_{\text{mode}}B_{21}h\nu, \quad P(h\nu)dv = N_{\text{mode}}h\nu N_m$$

Assuming only one mode

$$\frac{dN_m}{dz} = (N_2 - N_1)B_{21}h\nu N_m + B_{21}N_2 h\nu,$$

$$\frac{dN_m}{(N_2 - N_1)N_m + N_2} = B_{21}h\nu dz,$$

## Noise Power

$$\frac{dN_m}{N_m + \frac{N_2}{(N_2 - N_1)}} = B_{21} h\nu (N_2 - N_1) dz,$$

$$\frac{dN_m}{N_m + n_{sp}} = B_{21} h\nu (N_2 - N_1) dz, \quad n_{sp} = \frac{N_2}{N_2 - N_1}, \text{ is the spontaneous factor.}$$

$$\ln(N_m + n_{sp}) \Big|_0^L = B_{21} h\nu (N_2 - N_1) L,$$

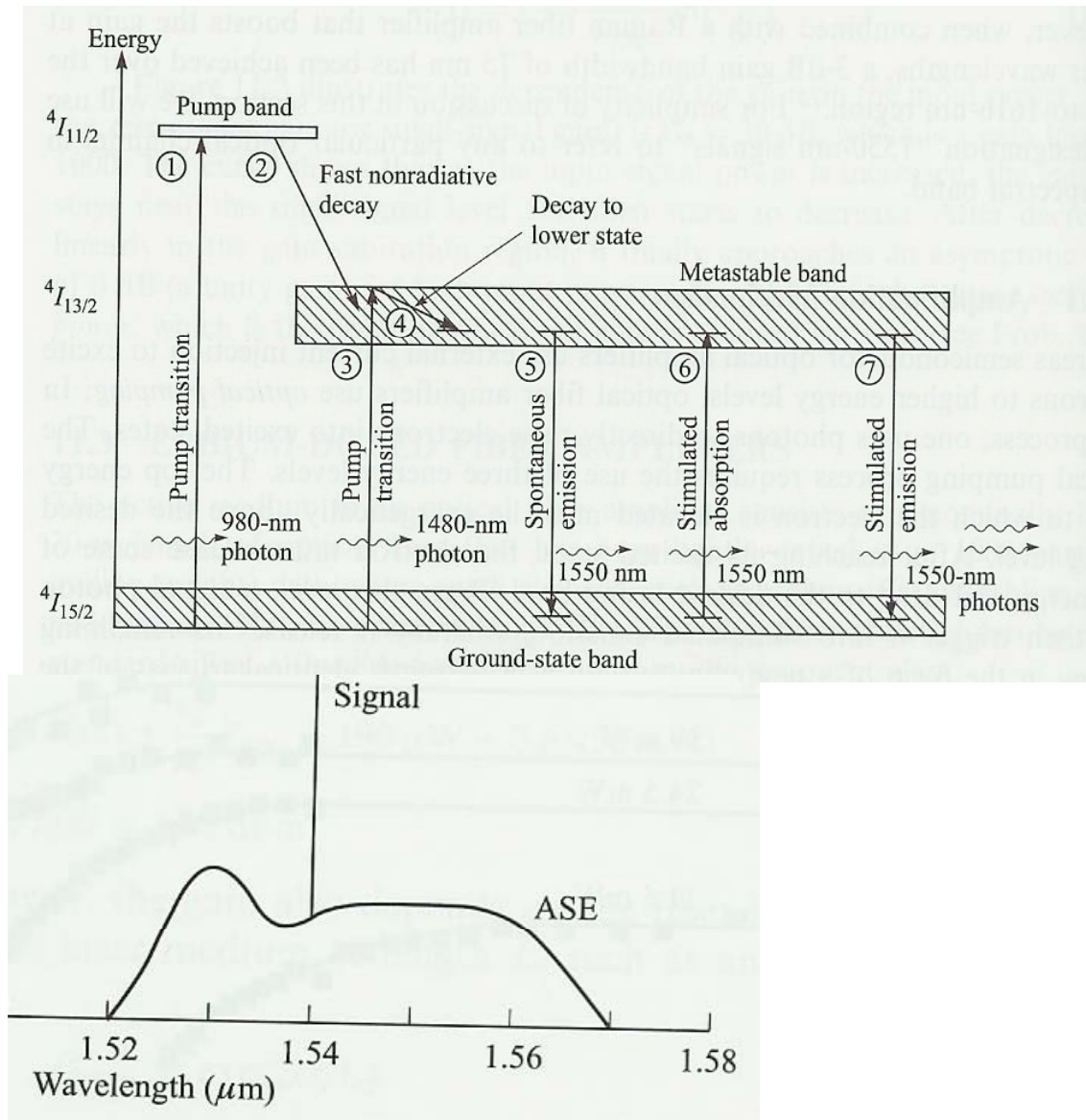
$$\frac{N_m(L) + n_{sp}}{N_m(0) + n_{sp}} = e^{gL} = G,$$

$$N_m(L) = N_m(0)G + n_{sp}(G - 1),$$

$$P_{ASE} = n_{sp}(G - 1)h\nu,$$

Power spectral density

## Amplified spontaneous noise



Noise Power spectral density:

$$S(\nu) = (G - 1)n_{sp}h\nu,$$

$$n_{sp} = \frac{N_2}{N_2 - N_1},$$

Total ASE power:

$$P_{ASE} = S(\nu)\Delta\nu = (G - 1)n_{sp}h\nu\Delta\nu,$$

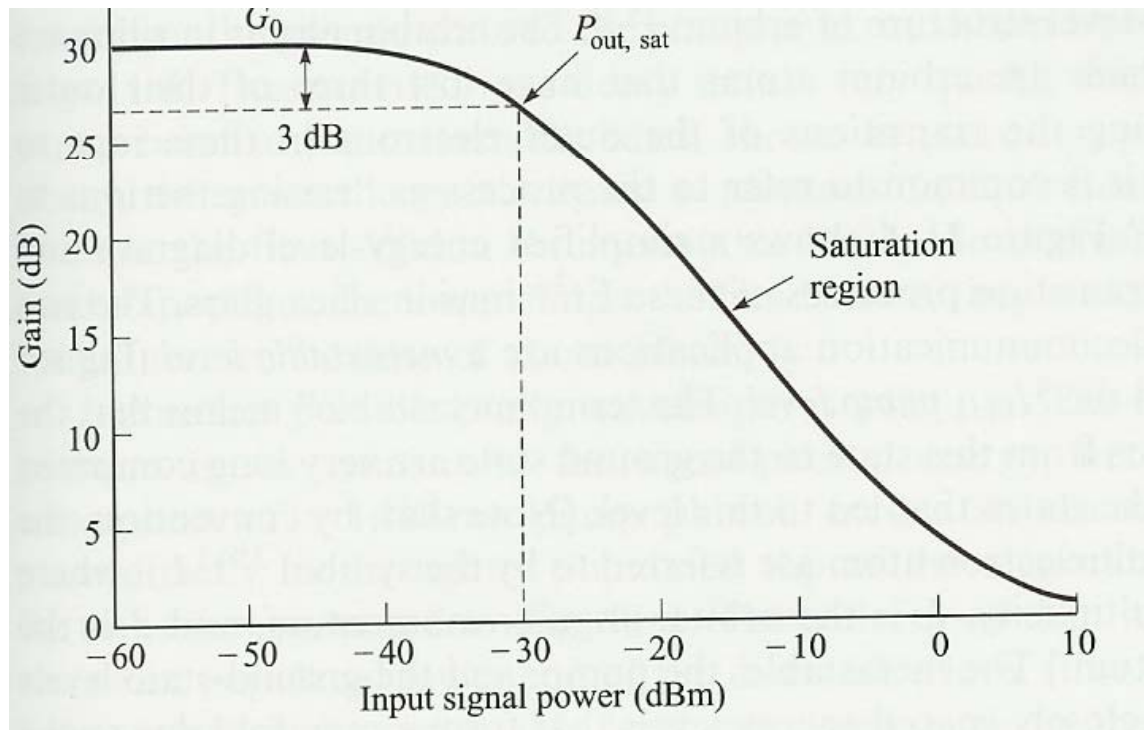
Total power:

$$P = P_{signal} + P_{ASE} = GP_{s,in} + S_{ASE}\Delta\nu,$$

## Total amplifier gain

$$G = \frac{P_{s,out}}{P_{s,in}} = \exp[(\Gamma g - \alpha)L], \quad g(z) = \frac{g_0}{1 + P_{s,in}(z)/P_{s,sat}} = \frac{1}{P_{s,in}(z)} \frac{dP_{s,in}(z)}{dz},$$

$$g_0 dz = \left[ \frac{dP_{s,in}(z)}{P_{s,in}(z)} + \frac{P_{s,in}(z)}{P_{s,sat}} \right], \quad \ln G = \ln G_0 + \frac{P_{s,out} - P_{s,in}}{P_{s,sat}}, \quad G = 1 + \frac{P_{s,sat}}{P_{s,in}} \ln\left(\frac{G_0}{G}\right),$$





## Amplifier Example

For an optical amplifier, when the input signal is 2.0mW, the output signal is 40mW. When the input is  $-28\text{dBm}$ , the output power is  $-10\text{dBm}$ . What's the maximum power can be extracted from the amplifier?

### Solution:

$$G_0 = 18\text{dB} = 63 = \exp(g_0 L), \quad \ln G = \ln G_0 + \frac{P_{s,out} - P_{s,in}}{P_{s,sat}},$$

$$g_0 L = 4.14, \quad \ln G = \ln\left(\frac{40}{2}\right) = \ln G_0 + \frac{40 - 2}{P_{s,sat}},$$

$$P_{s,sat} = 33.2\text{mW} / \text{cm}^2,$$

$$P_{\max} = g_0 L P_{s,sat},$$

## Receiver noise

Total photo-detector current:

$$i_{total} \propto (E_s + E_n)^2, \quad P = P_{signal} + P_{ASE} = GP_{s,in} + S_{ASE}\Delta\nu,$$

$$\langle i_{total,noise}^2 \rangle = \sigma_T^2 + \sigma_{shot-S}^2 + \sigma_{shot-ASE}^2 + \sigma_{S-ASE}^2 + \sigma_{ASE-ASE}^2,$$

$$\sigma_T^2 = \frac{4kT}{R}, \quad R \text{ is the resistance of the detector load resistor.}$$

$$\sigma_{S-ASE}^2 = 4\mathfrak{R}^2 P_{in} n_{sp} h\nu G(G-1)B_e,$$

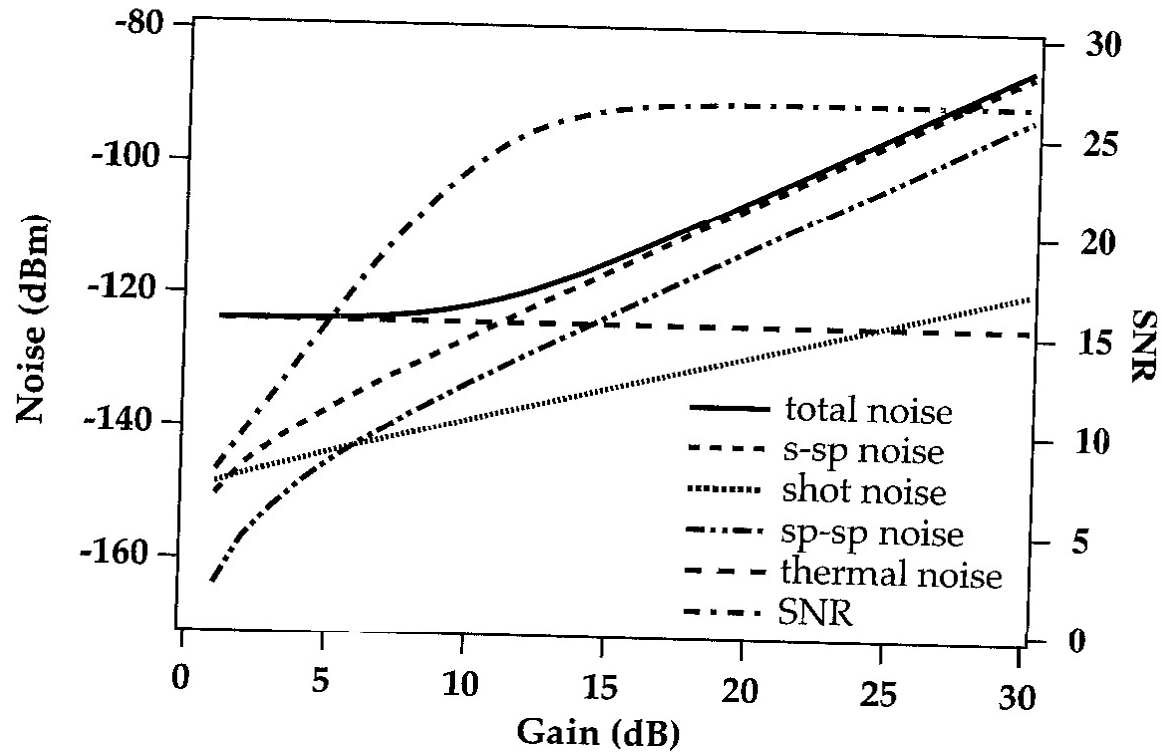
$$\sigma_{shot-S}^2 = 2e\mathfrak{R}GP_{in}B_e,$$

$$\left(\frac{S}{N}\right)_{out} = \frac{i_{ph}^2}{i_{noise}^2} = \frac{\mathfrak{R}P_{s,in}}{2eB_e} \frac{G}{1+2n_{sp}(G-1)}, \quad \left(\frac{S}{N}\right)_{in} = \frac{\mathfrak{R}P_{s,in}}{2eB_e},$$

$$NF = \frac{(S/N)_{in}}{(S/N)_{out}} = \frac{1+2n_{sp}(G-1)}{G} \approx 2n_{sp},$$

## Receiver noise

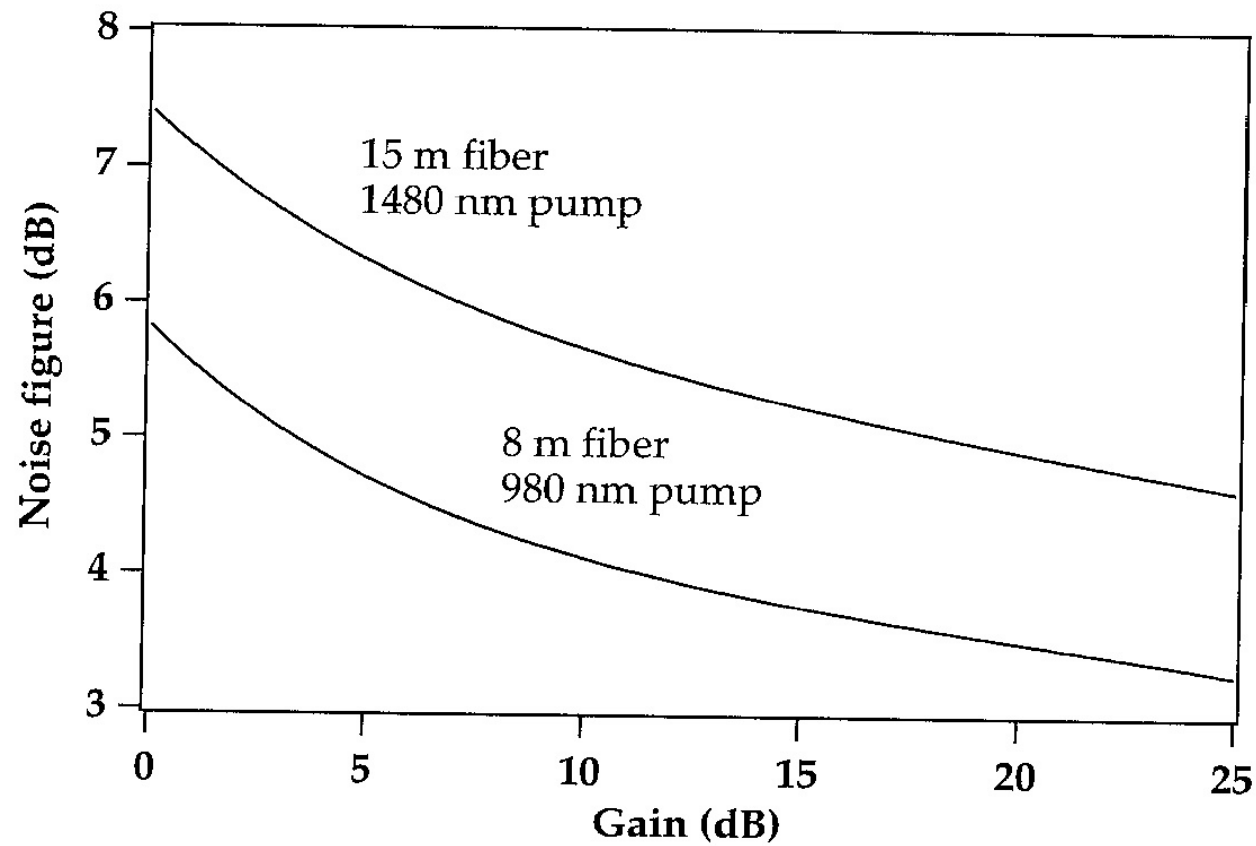
Total photo-detector current:



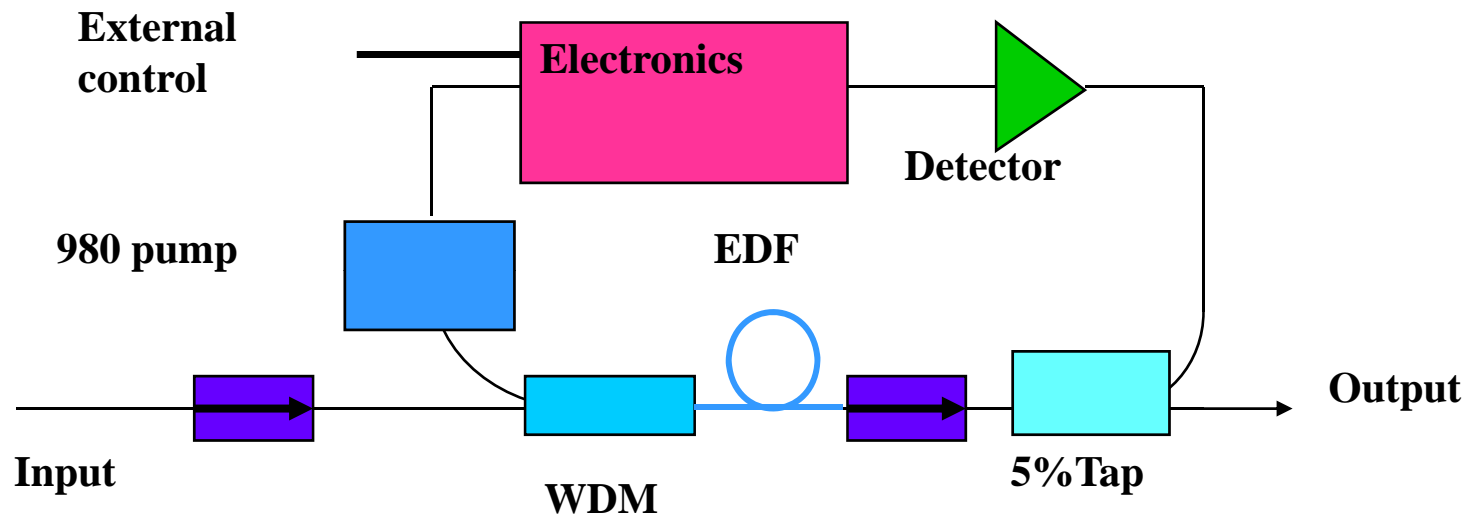
$$\langle i_{total,noise}^2 \rangle = \sigma_T^2 + \sigma_{short-S}^2 + \sigma_{short-ASE}^2 + \sigma_{S-ASE}^2 + \sigma_{ASE-ASE}^2,$$

## Gain and Noise Figure

Total photo-detector current:



## Amplifier System Noise figure (NF)



$$NF_{total} (dB) = NF_{OAP} (dB) + Loss_{input} (dB),$$