

in-phase  
 phase opposition  
 voltage maxima and minima  
 current maxima and minima  
 voltage standing-wave ratio (VSWR or SWR)  $S$   
 slotted line  
 input impedance  $Z_{in}$   
 short-circuited line  
 open-circuited line  
 quarter-wave transformer  
 Smith chart  
 unit circle  
 normalized impedance  
 normalized load resistance  $r_L$   
 normalized load reactance  $x_L$   
 WTG and WTL  
 SWR circle  
 admittance  $Y$   
 conductance  $G$  and susceptance  $B$   
 impedance matching  
 matching network  
 single-stub matching  
 transient response  
 bounce diagram

## PROBLEMS

### Sections 2-1 to 2-4: Transmission-Line Model

**2.1\*** A transmission line of length  $l$  connects a load to a sinusoidal voltage source with an oscillation frequency  $f$ . Assuming that the velocity of wave propagation on the line is  $c$ , for which of the following situations is it reasonable to ignore the presence of the transmission line in the solution of the circuit:

- (a)  $l = 20$  cm,  $f = 20$  kHz  
 (b)  $l = 50$  km,  $f = 60$  Hz

\*Answer(s) available in Appendix D.

• Solution available in CD-ROM.

(c)  $l = 20$  cm,  $f = 600$  MHz

(d)  $l = 1$  mm,  $f = 100$  GHz

**2.2** Calculate the line parameters  $R'$ ,  $L'$ ,  $G'$ , and  $C'$  for a coaxial line with an inner conductor diameter of 0.5 cm and an outer conductor diameter of 1 cm, filled with an insulating material where  $\mu = \mu_0$ ,  $\epsilon_r = 4.5$ , and  $\sigma = 10^{-3}$  S/m. The conductors are made of copper with  $\mu_c = \mu_0$  and  $\sigma_c = 5.8 \times 10^7$  S/m. The operating frequency is 1 GHz.

**2.3\*** A 1-GHz parallel-plate transmission line consists of 1.2-cm-wide copper strips separated by a 0.15-cm-thick layer of polystyrene. Appendix B gives  $\mu_c = \mu_0 = 4\pi \times 10^{-7}$  (H/m) and  $\sigma_c = 5.8 \times 10^7$  (S/m) for copper, and  $\epsilon_r = 2.6$  for polystyrene. Use Table 2-1 to determine the line parameters of the transmission line. Assume that  $\mu = \mu_0$  and  $\sigma \simeq 0$  for polystyrene.

**2.4** Show that the transmission-line model shown in Fig. 2-37 yields the same telegrapher's equations given by Eqs. (2.14) and (2.16).

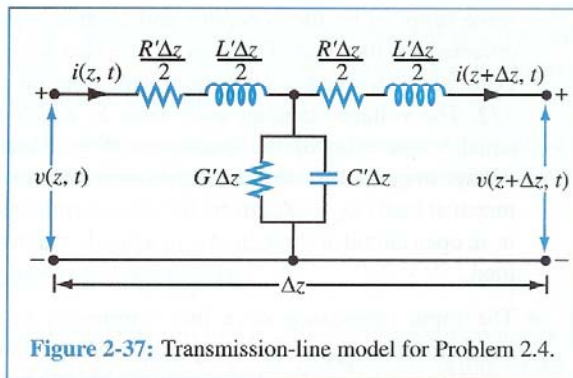


Figure 2-37: Transmission-line model for Problem 2.4.

**2.5\*** Find  $\alpha$ ,  $\beta$ ,  $u_p$ , and  $Z_0$  for the coaxial line of Problem 2.2.

## Section 2-5: The Lossless Line

2.6 In addition to not dissipating power, a lossless line has two important features: (1) it is dispersionless ( $u_p$  is independent of frequency); and (2) its characteristic impedance  $Z_0$  is purely real. Sometimes, it is not possible to design a transmission line such that  $R' \ll \omega L'$  and  $G' \ll \omega C'$ , but it is possible to choose the dimensions of the line and its material properties so as to satisfy the condition

$$R'C' = L'G' \quad (\text{distortionless line})$$

Such a line is called a *distortionless* line, because despite the fact that it is not lossless, it nonetheless possesses the previously mentioned features of the lossless line. Show that for a distortionless line,

$$\alpha = R' \sqrt{\frac{C'}{L'}} = \sqrt{R'G'}$$

$$\beta = \omega \sqrt{L'C'}$$

$$Z_0 = \sqrt{\frac{L'}{C'}}$$

2.7\* For a distortionless line [see Problem 2.6] with  $Z_0 = 50 \Omega$ ,  $\alpha = 20$  (mNp/m), and  $u_p = 2.5 \times 10^8$  (m/s), find the line parameters and  $\lambda$  at 100 MHz.

2.8 Find  $\alpha$  and  $Z_0$  of a distortionless line whose  $R' = 2 \Omega/\text{m}$  and  $G' = 2 \times 10^{-4}$  S/m.

2.9\* A transmission line operating at 125 MHz has  $Z_0 = 40 \Omega$ ,  $\alpha = 0.02$  (Np/m), and  $\beta = 0.75$  rad/m. Find the line parameters  $R'$ ,  $L'$ ,  $G'$ , and  $C'$ .

2.10 Using a slotted line, the voltage on a lossless transmission line was found to have a maximum magnitude of 1.5 V and a minimum magnitude of 0.6 V. Find the magnitude of the load's reflection coefficient.

2.11\* Polyethylene with  $\epsilon_r = 2.25$  is used as the insulating material in a lossless coaxial line with a characteristic impedance of  $50 \Omega$ . The radius of the inner conductor is 1.2 mm.

- What is the radius of the outer conductor?
- What is the phase velocity of the line?

2.12 A  $50\text{-}\Omega$  lossless transmission line is terminated in a load with impedance  $Z_L = (30 - j50) \Omega$ . The wavelength is 8 cm. Find the following:

- The reflection coefficient at the load.
- The standing-wave ratio on the line.
- The position of the voltage maximum nearest the load.
- The position of the current maximum nearest the load.

2.13\* On a  $150\text{-}\Omega$  lossless transmission line, the following observations were noted: distance of first voltage minimum from the load = 3 cm; distance of first voltage maximum from the load = 9 cm;  $S = 3$ . Find  $Z_L$ .

2.14 Using a slotted line, the following results were obtained: distance of first minimum from the load = 4 cm; distance of second minimum from the load = 14 cm; voltage standing-wave ratio = 1.5. If the line is lossless and  $Z_0 = 50 \Omega$ , find the load impedance.

2.15\* A load with impedance  $Z_L = (25 - j50) \Omega$  is to be connected to a lossless transmission line with characteristic impedance  $Z_0$ , with  $Z_0$  chosen such that the standing-wave ratio is the smallest possible. What should  $Z_0$  be?

2.16 A  $50\text{-}\Omega$  lossless line terminated in a purely resistive load has a voltage standing-wave ratio of 3. Find all possible values of  $Z_L$ .

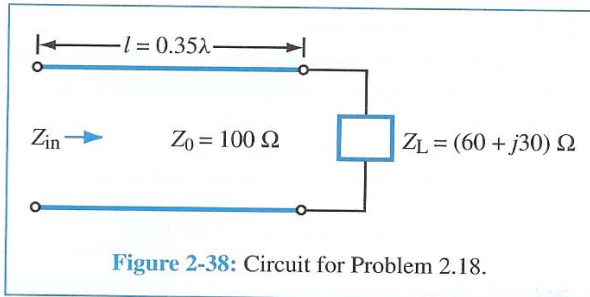


Figure 2-38: Circuit for Problem 2.18.

### Section 2-6: Input Impedance

**2.17\*** At an operating frequency of 300 MHz, a lossless 50- $\Omega$  air-spaced transmission line 2.5 m in length is terminated with an impedance  $Z_L = (40 + j20) \Omega$ . Find the input impedance.

**2.18** A lossless transmission line of electrical length  $l = 0.35\lambda$  is terminated in a load impedance as shown in Fig. 2-38. Find  $\Gamma$ ,  $S$ , and  $Z_{in}$ .

**2.19** Show that the input impedance of a quarter-wavelength-long lossless line terminated in a short circuit appears as an open circuit.

**2.20** Show that at the position where the magnitude of the voltage on the line is a maximum, the input impedance is purely real.

**2.21\*** A voltage generator with

$$v_g(t) = 5 \cos(2\pi \times 10^9 t) \text{ V}$$

and internal impedance  $Z_g = 50 \Omega$  is connected to a 50- $\Omega$  lossless air-spaced transmission line. The line length is 5 cm and it is terminated in a load with impedance  $Z_L = (100 - j100) \Omega$ . Find the following:

- $\Gamma$  at the load.
- $Z_{in}$  at the input to the transmission line.
- The input voltage  $\tilde{V}_i$  and input current  $\tilde{I}_i$ .

**2.22** A 6-m section of 150- $\Omega$  lossless line is driven by a source with

$$v_g(t) = 5 \cos(8\pi \times 10^7 t - 30^\circ) \text{ (V)}$$

and  $Z_g = 150 \Omega$ . If the line, which has a relative permittivity  $\epsilon_r = 2.25$ , is terminated in a load  $Z_L = (150 - j50) \Omega$ , find the following:

- $\lambda$  on the line.
- The reflection coefficient at the load.
- The input impedance.
- The input voltage  $\tilde{V}_i$ .
- The time-domain input voltage  $v_i(t)$ .

**2.23\*** Two half-wave dipole antennas, each with an impedance of 75  $\Omega$ , are connected in parallel through a pair of transmission lines, and the combination is connected to a feed transmission line, as shown in Fig. 2-39. All lines are 50  $\Omega$  and lossless.

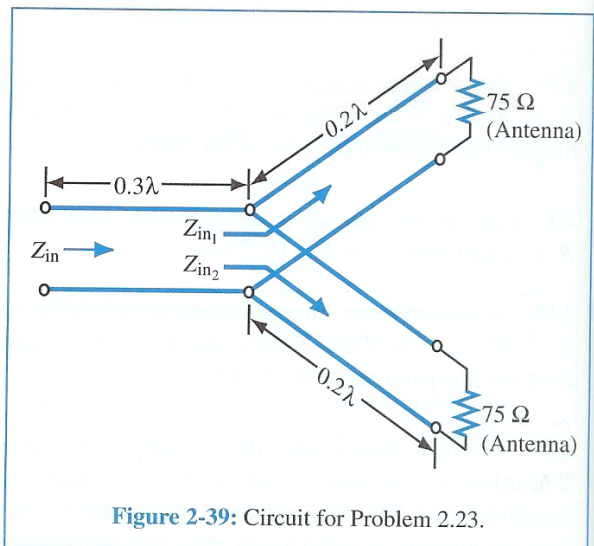


Figure 2-39: Circuit for Problem 2.23.



- (a) Calculate  $Z_{in_1}$ , the input impedance of the antenna-terminated line, at the parallel juncture.
- (b) Combine  $Z_{in_1}$  and  $Z_{in_2}$  in parallel to obtain  $Z'_L$ , the effective load impedance of the feedline.
- (c) Calculate  $Z_{in}$  of the feedline.

### Section 2-7: Special Cases

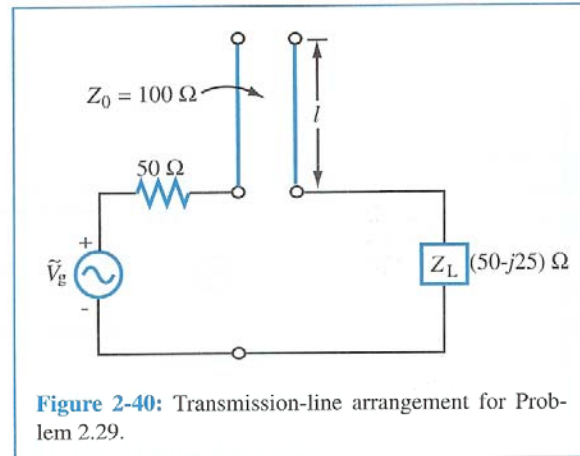
**2.24** At an operating frequency of 300 MHz, it is desired to use a section of a lossless 50- $\Omega$  transmission line terminated in a short circuit to construct an equivalent load with reactance  $X = 40 \Omega$ . If the phase velocity of the line is  $0.75c$ , what is the shortest possible line length that would exhibit the desired reactance at its input?

**2.25\*** A lossless transmission line is terminated in a short circuit. How long (in wavelengths) should the line be for it to appear as an open circuit at its input terminals?

**2.26** The input impedance of a 31-cm-long lossless transmission line of unknown characteristic impedance was measured at 1 MHz. With the line terminated in a short circuit, the measurement yielded an input impedance equivalent to an inductor with inductance of  $0.064 \mu\text{H}$ , and when the line was open-circuited, the measurement yielded an input impedance equivalent to a capacitor with capacitance of 40 pF. Find  $Z_0$  of the line, the phase velocity, and the relative permittivity of the insulating material.

**2.27\*** A 75- $\Omega$  resistive load is preceded by a  $\lambda/4$  section of a 50- $\Omega$  lossless line, which itself is preceded by another  $\lambda/4$  section of a 100- $\Omega$  line. What is the input impedance?

**2.28** A 100-MHz FM broadcast station uses a 300- $\Omega$  transmission line between the transmitter and a tower-mounted half-wave dipole antenna. The antenna impedance is 73  $\Omega$ . You are asked to design a quarter-wave transformer to match the antenna to the line.



**Figure 2-40:** Transmission-line arrangement for Problem 2.29.

- (a) Determine the electrical length and characteristic impedance of the quarter-wave section.
- (b) If the quarter-wave section is a two-wire line with  $d = 2.5 \text{ cm}$ , and the spacing between the wires is made of polystyrene with  $\epsilon_r = 2.6$ , determine the physical length of the quarter-wave section and the radius of the two wire conductors.

**2.29\*** A 50-MHz generator with  $Z_g = 50 \Omega$  is connected to a load  $Z_L = (50 - j25) \Omega$ . The time-average power transferred from the generator into the load is maximum when  $Z_g = Z_L^*$ , where  $Z_L^*$  is the complex conjugate of  $Z_L$ . To achieve this condition without changing  $Z_g$ , the effective load impedance can be modified by adding an open-circuited line in series with  $Z_L$ , as shown in Fig. 2-40. If the line's  $Z_0 = 100 \Omega$ , determine the shortest length of line (in wavelengths) necessary for satisfying the maximum-power-transfer condition.

**2.30** A 50- $\Omega$  lossless line of length  $l = 0.375\lambda$  connects a 300-MHz generator with  $\tilde{V}_g = 300 \text{ V}$  and  $Z_g = 50 \Omega$  to a load  $Z_L$ . Determine the time-domain current through the load for:

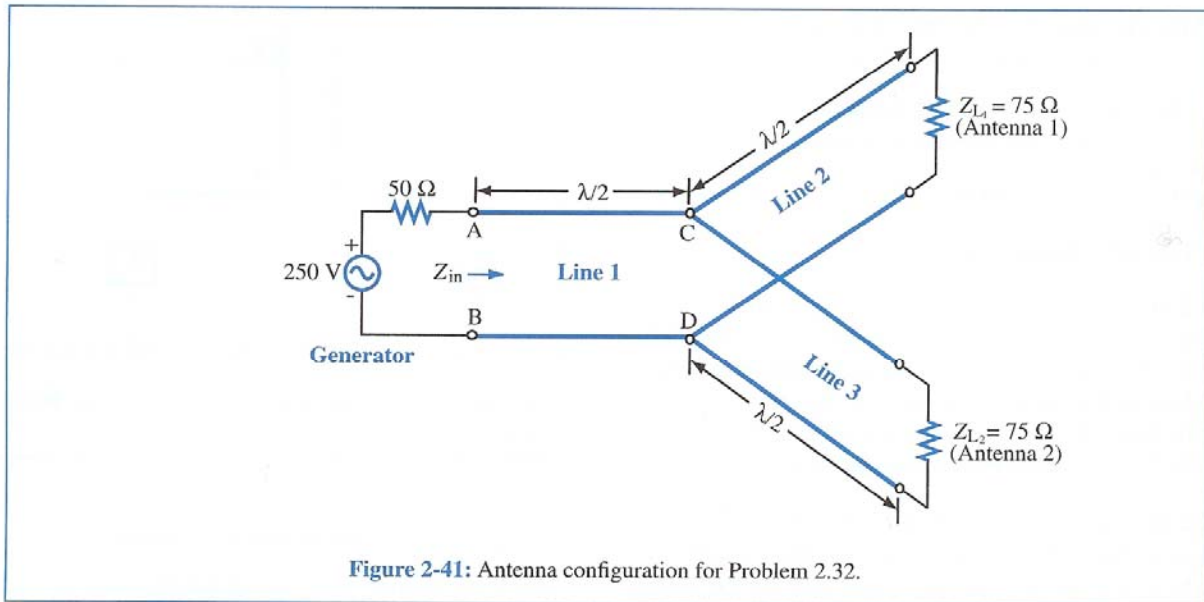


Figure 2-41: Antenna configuration for Problem 2.32.

- (a)  $Z_L = (50 - j50) \Omega$
- (b)  $Z_L = 50 \Omega$
- (c)  $Z_L = 0$  (short circuit)

### Section 2-8: Power Flow on Lossless Line

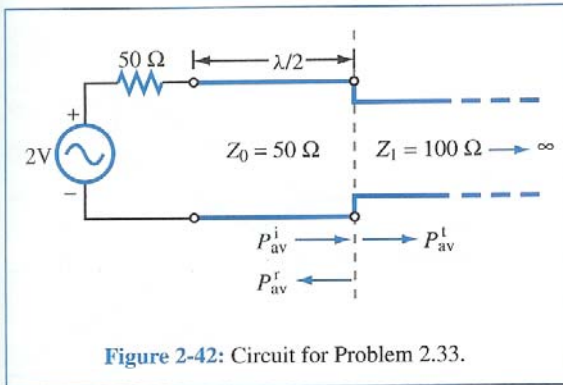
**2.31\*** A generator with  $\tilde{V}_g = 300$  V and  $Z_g = 50 \Omega$  is connected to a load  $Z_L = 75 \Omega$  through a  $50\text{-}\Omega$  lossless line of length  $l = 0.15\lambda$ .

- (a) Compute  $Z_{in}$ , the input impedance of the line at the generator end.
- (b) Compute  $\tilde{I}_i$  and  $\tilde{V}_i$ .
- (c) Compute the time-average power delivered to the line,  $P_{in} = \frac{1}{2} \Re\{\tilde{V}_i \tilde{I}_i^*\}$ .

- (d) Compute  $\tilde{V}_L$ ,  $\tilde{I}_L$ , and the time-average power delivered to the load,  $P_L = \frac{1}{2} \Re\{\tilde{V}_L \tilde{I}_L^*\}$ . How does  $P_{in}$  compare to  $P_L$ ? Explain.
- (e) Compute the time-average power delivered by the generator,  $P_g$ , and the time-average power dissipated in  $Z_g$ . Is conservation of power satisfied?

**2.32** If the two-antenna configuration shown in Fig. 2-41 is connected to a generator with  $\tilde{V}_g = 250$  V and  $Z_g = 50 \Omega$ , how much average power is delivered to each antenna?

**2.33\*** For the circuit shown in Fig. 2-42, calculate the average incident power, the average reflected power, and the average power transmitted into the infinite  $100\text{-}\Omega$  line. The  $\lambda/2$  line is lossless and the infinitely long line is slightly lossy. (Hint: The input impedance of an infinitely long line is equal to its characteristic impedance so long as  $\alpha \neq 0$ .)



**2.34** An antenna with a load impedance

$$Z_L = (75 + j25) \Omega$$

is connected to a transmitter through a 50-Ω lossless transmission line. If under matched conditions (50-Ω load) the transmitter can deliver 20 W to the load, how much power can it deliver to the antenna? Assume that  $Z_g = Z_0$ .

**Section 2-9: Smith Chart**

**2.35\*** Use the Smith chart to find the reflection coefficient corresponding to a load impedance of

- (a)  $Z_L = 3Z_0$
- ⊛ (b)  $Z_L = (2 - 2j)Z_0$
- (c)  $Z_L = -2jZ_0$
- (d)  $Z_L = 0$  (short circuit)

**2.36** Use the Smith chart to find the normalized load impedance corresponding to a reflection coefficient of

- (a)  $\Gamma = 0.5$
- ⊛ (b)  $\Gamma = 0.5 \angle 60^\circ$
- (c)  $\Gamma = -1$

- (d)  $\Gamma = 0.3 \angle -30^\circ$
- (e)  $\Gamma = 0$
- (f)  $\Gamma = j$

**2.37\*** On a lossless transmission line terminated in a load  $Z_L = 100 \Omega$ , the standing-wave ratio was measured to be 2.5. Use the Smith chart to find the two possible values of  $Z_0$ .

**2.38** A lossless 50-Ω transmission line is terminated in a load with  $Z_L = (50 + j25) \Omega$ . Use the Smith chart to find the following:

- (a) The reflection coefficient  $\Gamma$ .
- (b) The standing-wave ratio.
- (c) The input impedance at  $0.35\lambda$  from the load.
- (d) The input admittance at  $0.35\lambda$  from the load.
- (e) The shortest line length for which the input impedance is purely resistive.
- (f) The position of the first voltage maximum from the load.

**2.39\*** A lossless 50-Ω transmission line is terminated in a short circuit. Use the Smith chart to find the following:

- (a) The input impedance at a distance  $2.3\lambda$  from the load.
- (b) The distance from the load at which the input admittance is  $Y_{in} = -j0.04 \text{ S}$ .

**2.40** Use the Smith chart to find  $y_L$  if  $z_L = 1.5 - j0.7$ .

**2.41\*** A lossless 100-Ω transmission line  $3\lambda/8$  in length is terminated in an unknown impedance. If the input impedance is  $Z_{in} = -j2.5 \Omega$ ,

- (a) Use the Smith chart to find  $Z_L$ .
- (b) What length of open-circuit line could be used to replace  $Z_L$ ?



**2.42** A  $75\text{-}\Omega$  lossless line is  $0.6\lambda$  long. If  $S = 1.8$  and  $\theta_r = -60^\circ$ , use the Smith chart to find  $|\Gamma|$ ,  $Z_L$ , and  $Z_{in}$ .

**2.43\*** Using a slotted line on a  $50\text{-}\Omega$  air-spaced lossless line, the following measurements were obtained:  $S = 1.6$  and  $|\tilde{V}|_{\max}$  occurred only at 10 cm and 24 cm from the load. Use the Smith chart to find  $Z_L$ .

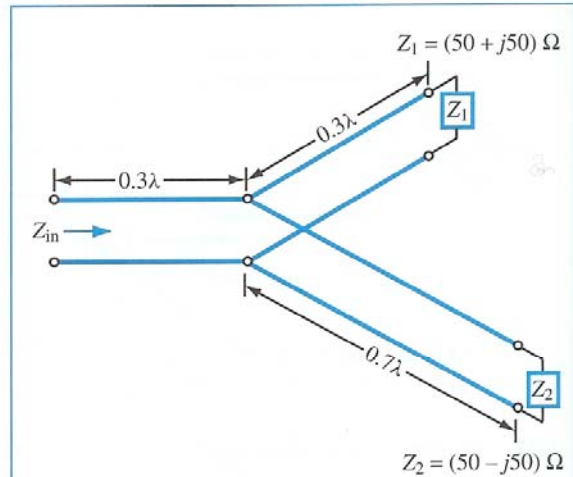
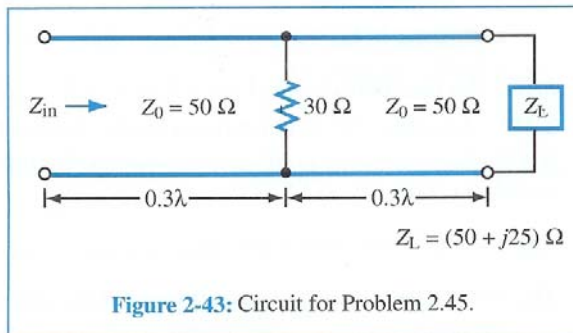
**2.44** At an operating frequency of 5 GHz, a  $50\text{-}\Omega$  lossless coaxial line with insulating material having a relative permittivity  $\epsilon_r = 2.25$  is terminated in an antenna with an impedance  $Z_L = 150\ \Omega$ . Use the Smith chart to find  $Z_{in}$ . The line length is 30 cm.

### Section 2-10: Impedance Matching

**2.45\*** A  $50\text{-}\Omega$  lossless line  $0.6\lambda$  long is terminated in a load with  $Z_L = (50 + j25)\ \Omega$ . At  $0.3\lambda$  from the load, a resistor with resistance  $R = 30\ \Omega$  is connected as shown in Fig. 2-43. Use the Smith chart to find  $Z_{in}$ .

**2.46** A  $50\text{-}\Omega$  lossless line is to be matched to an antenna with  $Z_L = (75 - j20)\ \Omega$  using a shorted stub. Use the Smith chart to determine the stub length and distance between the antenna and stub.

**2.47\*** Repeat Problem 2.46 for a load with  $Z_L = (100 + j50)\ \Omega$ .



**2.48** Use the Smith chart to find  $Z_{in}$  of the feed line shown in Fig. 2-44. All lines are lossless with  $Z_0 = 50\ \Omega$ .

**2.49\*** Repeat Problem 2.48 for the case where all three transmission lines are  $\lambda/4$  in length.

### Section 2-11: Transients on Transmission Lines

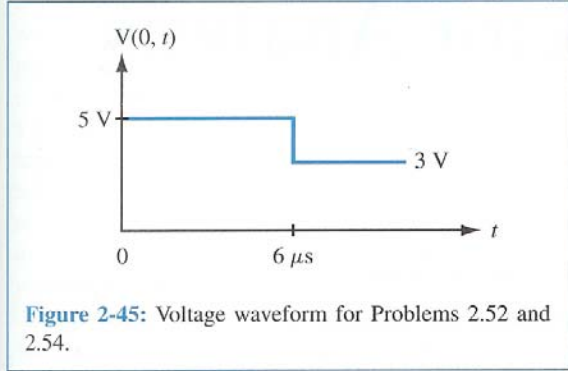
**2.50** Generate a bounce diagram for the voltage  $V(z, t)$  for a 1-m-long lossless line characterized by  $Z_0 = 50\ \Omega$  and  $u_p = 2c/3$  (where  $c$  is the velocity of light) if the line is fed by a step voltage applied at  $t = 0$  by a generator circuit with  $V_g = 60\ \text{V}$  and  $R_g = 100\ \Omega$ . The line is terminated in a load  $Z_L = 25\ \Omega$ . Use the bounce diagram to plot  $V(t)$  at a point midway along the length of the line from  $t = 0$  to  $t = 25\ \text{ns}$ .

**2.51** Repeat Problem 2.50 for the current  $I$  on the line.

**2.52** In response to a step voltage, the voltage waveform shown in Fig. 2-45 was observed at the sending end of a

lossless transmission line with  $R_g = 50 \Omega$ ,  $Z_0 = 50 \Omega$ , and  $\epsilon_r = 2.25$ . Determine the following:

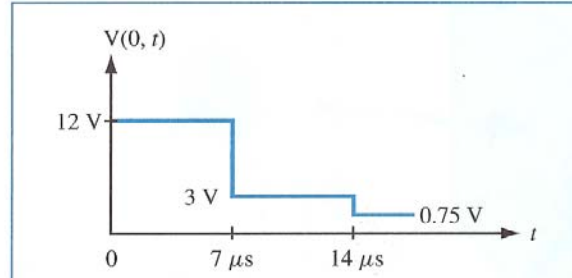
- (a) The generator voltage.
- (b) The length of the line.
- (c) The load impedance.



**2.53\*** In response to a step voltage, the voltage waveform shown in Fig. 2-46 was observed at the sending end of a shorted line with  $Z_0 = 50 \Omega$  and  $\epsilon_r = 4$ . Determine  $V_g$ ,  $R_g$ , and the line length.

**2.54** Suppose the voltage waveform shown in Fig. 2-45 was observed at the sending end of a  $50\text{-}\Omega$  transmission line in response to a step voltage introduced by a generator with  $V_g = 15 \text{ V}$  and an unknown series resistance  $R_g$ . The line is 1 km in length, its velocity of propagation is  $1 \times 10^8 \text{ m/s}$ , and it is terminated in a load  $Z_L = 100 \Omega$ .

- (a) Determine  $R_g$ .
- (b) Explain why the drop in level of  $V(0, t)$  at  $t = 6 \mu\text{s}$  cannot be due to reflection from the load.
- (c) Determine the shunt resistance  $R_f$  and location of the fault responsible for the observed waveform.



**Figure 2-46:** Voltage waveform of Problem 2.53.

**2.55** A generator circuit with  $V_g = 200 \text{ V}$  and  $R_g = 25 \Omega$  was used to excite a  $75\text{-}\Omega$  lossless line with a rectangular pulse of duration  $\tau = 0.4 \mu\text{s}$ . The line is 200 m long, its  $u_p = 2 \times 10^8 \text{ m/s}$ , and it is terminated in a load  $Z_L = 125 \Omega$ .

- (a) Synthesize the voltage pulse exciting the line as the sum of two step functions,  $V_{g1}(t)$  and  $V_{g2}(t)$ .
- (b) For each voltage step function, generate a bounce diagram for the voltage on the line.
- (c) Use the bounce diagrams to plot the total voltage at the sending end of the line.

**2.56** For the circuit of Problem 2.55, generate a bounce diagram for the current and plot its time history at the middle of the line.

**2.57–2.65** Additional Solved Problems — complete solutions on